Ardea Resources Limited

High-grade nickel-cobalt mineralization extended at Goongarrie

ASX & Media Release

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ASX Symbol

ARL

Ardea Resources Limited

Suite 2 / 45 Ord St
West Perth WA 6005

PO Box 1433
West Perth WA 6872

Telephone

+61 8 6244 5136

Email

ardea@ardearesources.com.au

Website

www.ardearesources.com.au

Directors

Katina Law
Executive Chair

Ian Buchhorn
Technical Executive Director

Wayne Bramwell
Non-Executive Director

Issued Capital

Fully Paid Ordinary Shares
104,990,413

Unlisted options exercisable at $0.25
12,310,022

Directors/Employee Performance Rights
3.240,000

ABN 30 614 289 342

Recent drilling results from the Pamela Jean Deeps confirm and extend the deeper high-grade mineralization. This zone is scheduled as the mining target during the payback period, to enhance project economics.

- Ongoing Definitive Feasibility Study (DFS) drilling program confirms high-grade intercepts at the Pamela Jean Deeps orebody.
  - **AGSR419 112m at 1.30% Ni, 0.26% Co, 31g/t Sc from 30m**[1]
  - **AGSD0001 100.8m at 1.00% Ni, 0.08% Co from 32m**[2]
  - **AGSR0413 76m at 1.11% Ni, 0.09% Co and 38g/t Sc from 24m**
  - **AGSR0418 56m at 1.29% Ni, 0.14% Co and 18g/t Sc 104m**
  - **AGSR0190 57m at 1.04% Ni, 0.10% Co and 21g/t Sc from 70m**
- The top of Pamela Jean is a typical flat laterite surface at 15-30m below surface. Rather than a flat base some 40-50m below surface, the base of Pamela Jean is "funnel-shaped", penetrating up to 165m below surface. With continuous mineralisation to depth, this geometry fortuitously mimics pit design batters, minimizing Pamela Jean strip ratios. The result is high tonnes and grade proximal to future plant site.
- The "deep funnel" ore is associated with a narrow dyke and intense shearing that has facilitated exceptionally deep weathering (to 165m).
- An additional "funnel-shaped" Deeps ore zone discovered in 20m infill drilling (AGSR0190), suggests potential for further deeper high-grade ore, associated with bedrock structures, still requiring drill appraisal.
- Uniform goethite mineralization confirmed at Pamela Jean, validates Pamela Jean as a premium autoclave feed for project payback.
- Ore geometry very consistent, with >0.5% Ni pervasive between the base of lateritized alluvium overburden and top of carbonated saprock basement, facilitates predictable mine planning, free-dig ore until mining encounters sub-grade hard saprock at the pit base and within batters, excellent visual grade control.
- Ardea inclined drill-holes have precisely confirmed historic drill results, serves as a QAQC program for historic work.
- Scandium mineralization evident from surface, typically 30-62g/t Sc when occurring in the nickel-cobalt ore feed.
- Magnesite neutralizer pervasive within ore footwall, ~0.5% Ni credit.

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[1] Calculated using a 0.5 % nickel cut-off, 2 m minimum intercept, and 4 m maximum internal waste
[2] 0.5 % nickel cut-off, 2m minimum intercept, and 4m maximum intern waste, previous report 2017 core hole

Recent drilling results from the Goongarrie orebody

Pamela Jean Deeps

Significant intercepts from the Pamela Jean Deeps drilling[3]

6669440mN section			
	AGSR0412		38m at 0.89% nickel, 0.06% cobalt and 36g/t scandium from 22m[4]
		including	***8m at 1.16% nickel, 0.13% cobalt** and 34g/t scandium from 30*m
	AGSR0412		14m at 0.78% nickel, 0.04% cobalt and 8g/t scandium from 136m[4]
		including	*2m at 1.13% nickel, 0.11% cobalt and 6g/t scandium from 140m*
	AGSR0411		32m at 0.84% nickel, 0.05% cobalt and 15g/t scandium from 22m[4]
		including	*2m at 1.28% nickel, 0.09% cobalt and 22g/t scandium from 38m*
	AGSR0411		20m at 0.71% nickel, 0.03% cobalt and 9g/t scandium from 76m[4]
6669520mN section			
	AGSR0414		**4m at 0.44% nickel, 0.54% cobalt** and 52g/t scandium from 14m[4]
	AGSR0414		**38m at 1.01% nickel, 0.10% cobalt** and 43g/t scandium from 16m[4]
		including	***8m at 1.40% nickel**, 0.08% cobalt and 30g/t scandium from 40m*
	AGSR0413		**76m at 1.11% nickel, 0.09% cobalt** and 38g/t scandium from 24m[4]
		including	***12m at 1.11% nickel, 0.12% cobalt** and 36g/t scandium from 44m*
		including	***16m at 1.36% nickel, 0.22% cobalt** and 35g/t scandium from 66m*
		including	***4m at 1.36% nickel, 0.13% cobalt** and 33g/t scandium from 88m*
6669600mN section			
	AGSR0418		42m at 0.67% nickel, 0.04% cobalt and 14g/t scandium from 30m[4]
		including	*2m at 1.12% nickel, 0.09% cobalt and 13g/t scandium from 48m*
	AGSR0418		**56m at 1.29% nickel**, **0.14% cobalt** and 18g/t scandium from 104m[4]
		including	***36m at 1.40% nickel, 0.20% cobalt** and 19g/t scandium from 110m*
	AGSD0001		**100.8m at 1.00% nickel, 0.08% cobalt** from 34m[4]
		including	*2m at 1.02% nickel, 0.11% cobalt from 87m*
		including	***7.2m at 1.30% nickel, 0.45% cobalt** from 95.6m*
		including	***6m at 1.40% nickel, 0.22% cobalt** from 118m*

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[3] Drill-holes for the Pamela Jean deposit are listed first by section (south to north, then by hole west to east)
[4] Calculated using a 0.50 % nickel cut-off, 2 m minimum intercept, and 4 m maximum internal waste, for "including" intercept 0.08% Co cut-off

AGSD0001		**24.8m at 1.10% nickel**, 0.08% cobalt from 140.2m[4]
	including	***8m at 1.40% nickel, 0.11% cobalt** from 152m*
6669680mN section		
AGSR0419		**112m at 1.30% nickel, 0.26% cobalt** and 31g/t scandium from 30m[4]
	including	***6m at 1.14% nickel**, 0.08% cobalt and 19g/t scandium from 42m*
	including	***68m at 1.58% nickel, 0.39% cobalt** and 35g/t scandium from 72m*
6669760mN section		
AGSR0422		48m at 0.94% nickel, 0.07% cobalt and 19g/t scandium from 104m[4]
	including	*8m at 0.88% nickel, 0.16% cobalt and 18g/t scandium from 114m*
	including	*4m at 1.48% nickel, 0.09% cobalt and 135g/t scandium from 134m*
AGSR0421		26m at 0.66% nickel, 0.04% cobalt and 35g/t scandium from 20m[4]
AGSR0421		76m at 0.82% nickel, 0.07% cobalt and 28g/t scandium from 54m[4]
	including	***28m at 0.91% nickel, 0.14% cobalt** and 27g/t scandium from 84m*
AGSR0190		24m at 0.86% nickel, 0.02% cobalt and 99g/t scandium from 36m[4]
AGSR0190		**57m at 1.04% nickel, 0.10% cobalt** and 21g/t scandium from 70m
	including	***14m at 0.82% nickel, 0.20% cobalt** and 24g/t scandium from 70m*
	including	***16m at 1.28% nickel, 0.10% cobalt** and 29g/t scandium from 90m*
6669840mN section		
AGSR0186		**62m at 0.92% nickel**, 0.04% cobalt and 32g/t scandium from 22m[4]
	including	*2m at 1.40% nickel, 0.08% cobalt and 50g/t scandium from 66m*
AGSR0417		26m at 0.90% nickel, 0.04% cobalt and 29g/t scandium from 22m[4]
AGSR0187		**60m at 1.14% nickel**, 0.08% cobalt and 47g/t scandium from 24m[4]
	including	***24m at 1.27% nickel, 0.14% cobalt** and 33g/t scandium from 60m*
6669880mN section		
AGSR0416		28m at 0.87% nickel, 0.08% cobalt and 34g/t scandium from 62m[4]
	including	*4m at 0.83% nickel, 0.11% cobalt and 34g/t scandium from 62m*
	including	*8m at 0.91% nickel, 0.09% cobalt and 34g/t scandium from 82m*
6669920mN section		
AGSR0294		**18m at 0.98% nickel**, 0.08% cobalt and 34g/t scandium from 18m[4]
	including	*8m at 0.98% nickel, 0.12% cobalt and 43g/t scandium from 18m*
AGSR0415		**46m at 1.03% nickel**, 0.06% cobalt and 35g/t scandium from 28m[4]
	including	***10m at 1.33% nickel, 0.14% cobalt** and 34g/t scandium from 46m*

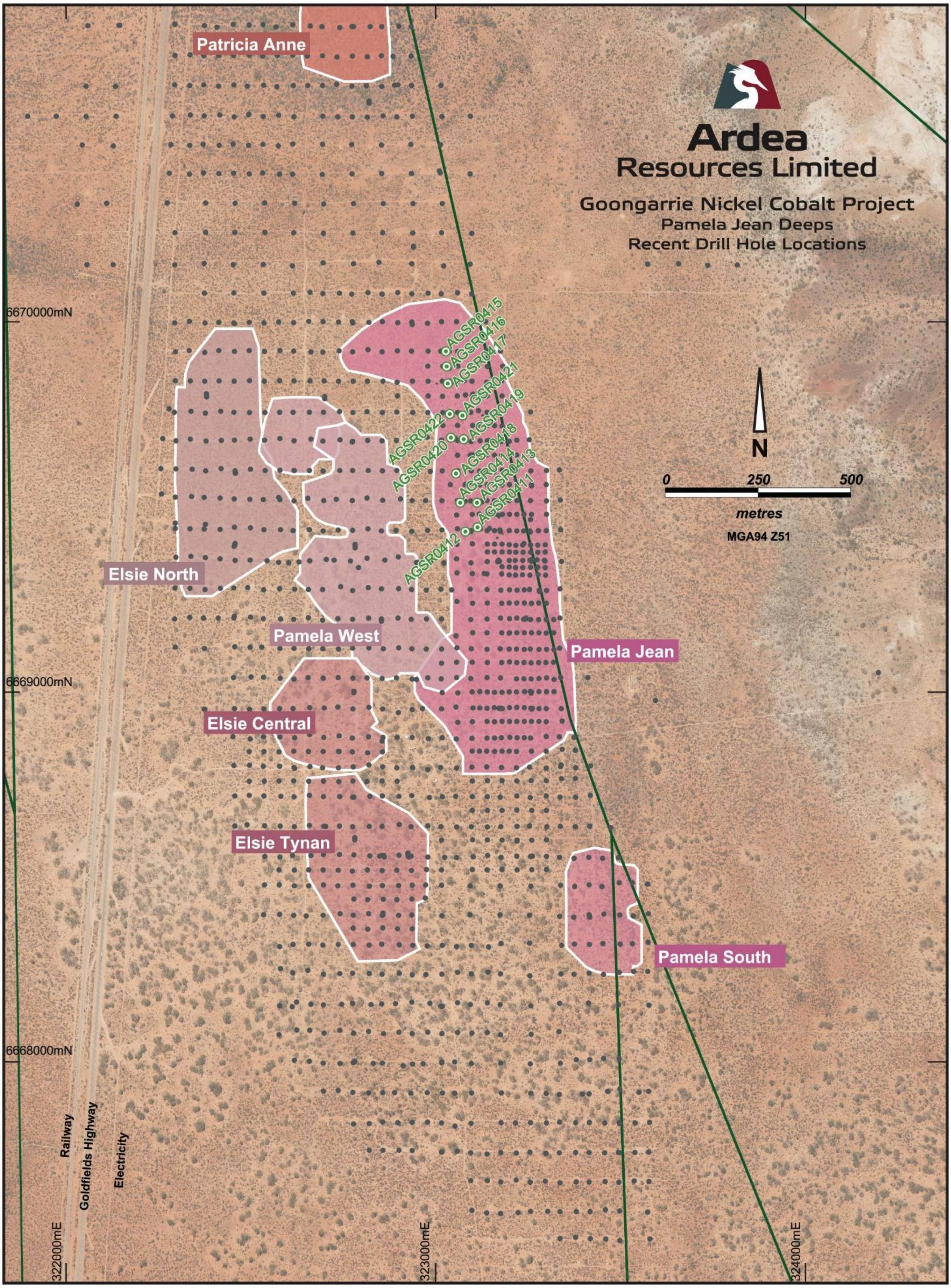
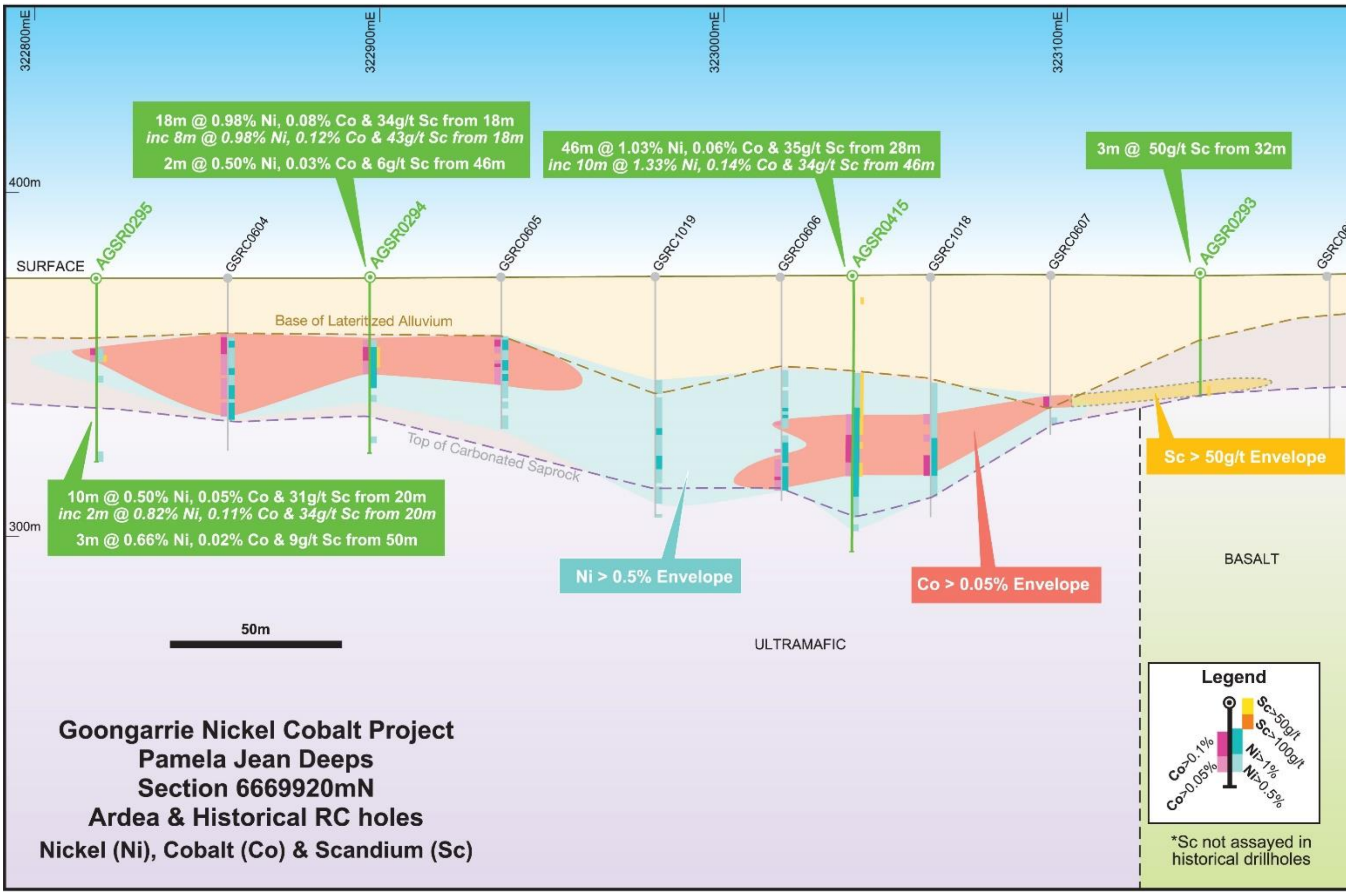


Figure 1 – Location of Ardea RC drilling (green & white dots and hole number). Dark dots show historic drill collars. Deposits are marked by significant nickel and cobalt mineralization and are encased within the overall nickel envelope (scheduled pits coloured pink, nominally Ni>0.5%, containing zones with Co>0.1%).



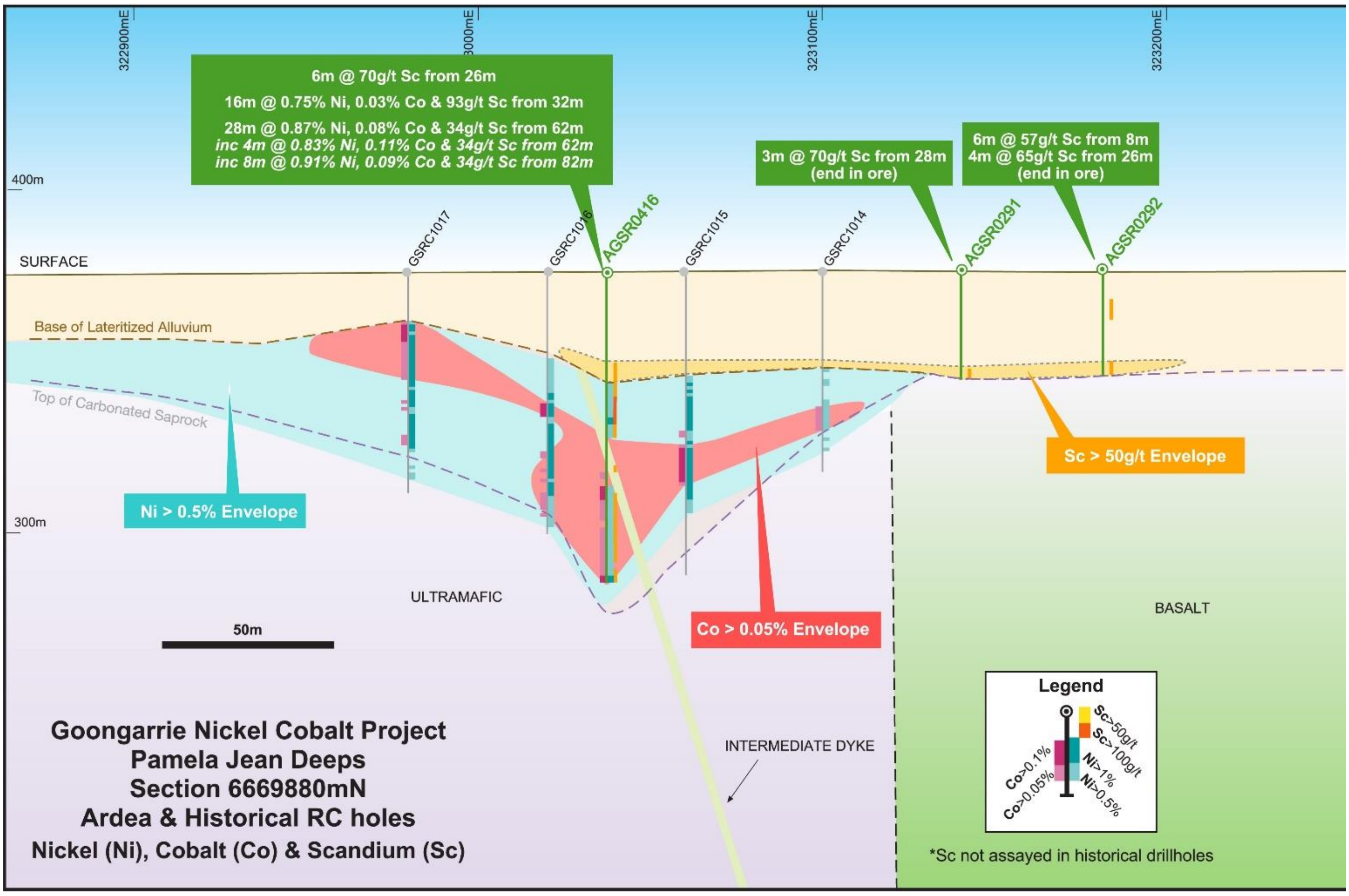


Figure 2 *Section 6669920mN* *Figure 3* *Section 6669880mN*

Pamela Jean Geological Model

The current Pamela Jean Deeps drilling was initially executed as a precursor to a geotechnical program, but has generated new insights into Goongarrie geological models, geo-metallurgy and geotechnics.

The 2018 Ardea drilling at Goongarrie, and Pamela Jean in particular, is restricted to 80x40m infill of proposed pit locations where existing 80x80m drill patterns define the current Indicated Mineral Resource (refer ASX announcement 14 March 2018 for current resource statement). Being infill drilling during 2018, changes to the overall Mineral Resources are expected to be non-material. Of note, historical geological interpretations for the run-of-mine "shallow flat" lateritic mineralization have been precisely confirmed by 2018 drilling, suggesting robust QAQC for historic Goongarrie drilling.

The recent Pamela Jean Deeps drilling has been different to earlier 2018 drilling, in that the inclined holes (first time executed anywhere at Goongarrie) have quantified deep "funnel-shaped" ore zones, especially in respect to structural controls on deep ore. Importantly, "deep funnel" mineralization has been defined (notably by drill-hole AGSR0190 section 6669760mN) where previous drilling only had "shallow flat" ore.

Historic hole GSRC0184 (323096mE) returned 22m at 0.58% Ni and 0.03% Co from 17m and GSRC1005 (323140mE) returned 35m at 0.82% Ni and 0.11% Co from 28m. Ardea RC drill-hole **AGSR0190** (323116mE) between the two returned **91m at 0.92% Ni and 0.07% Co** from 36m (stops in ore), and in addition intersected a previously unrecognized dyke dipping 65^0 east that fingerprints the "deep funnel".

Following this result, a systematic drill data review was completed, identifying a significant number of holes stopping in ore where potential deep "funnels" could be present (as for AGSR0190). This will necessitate amendments to wireframes and ultimately pit designs. With the deepening and widening of potential pits, various geotechnical parameters in terms of batter designs and PAL plant neutralizer also come into play.

As 2018 RC drilling winds down, data is being consolidated for current DFS programs. In particular, a geological model has been developed for Goongarrie which consolidates the current 575 holes for 26,528m of Ardea RC drilling with existing 2,372 holes for 115,384m of historical RC drilling. The Ardea model focuses on the mineralized regolith (the weathered mantle), and its relationship to the underlying protolith (the unweathered ultramafic bedrock). In particular, there is a marked bedrock structural control on overlying laterite mineralization.

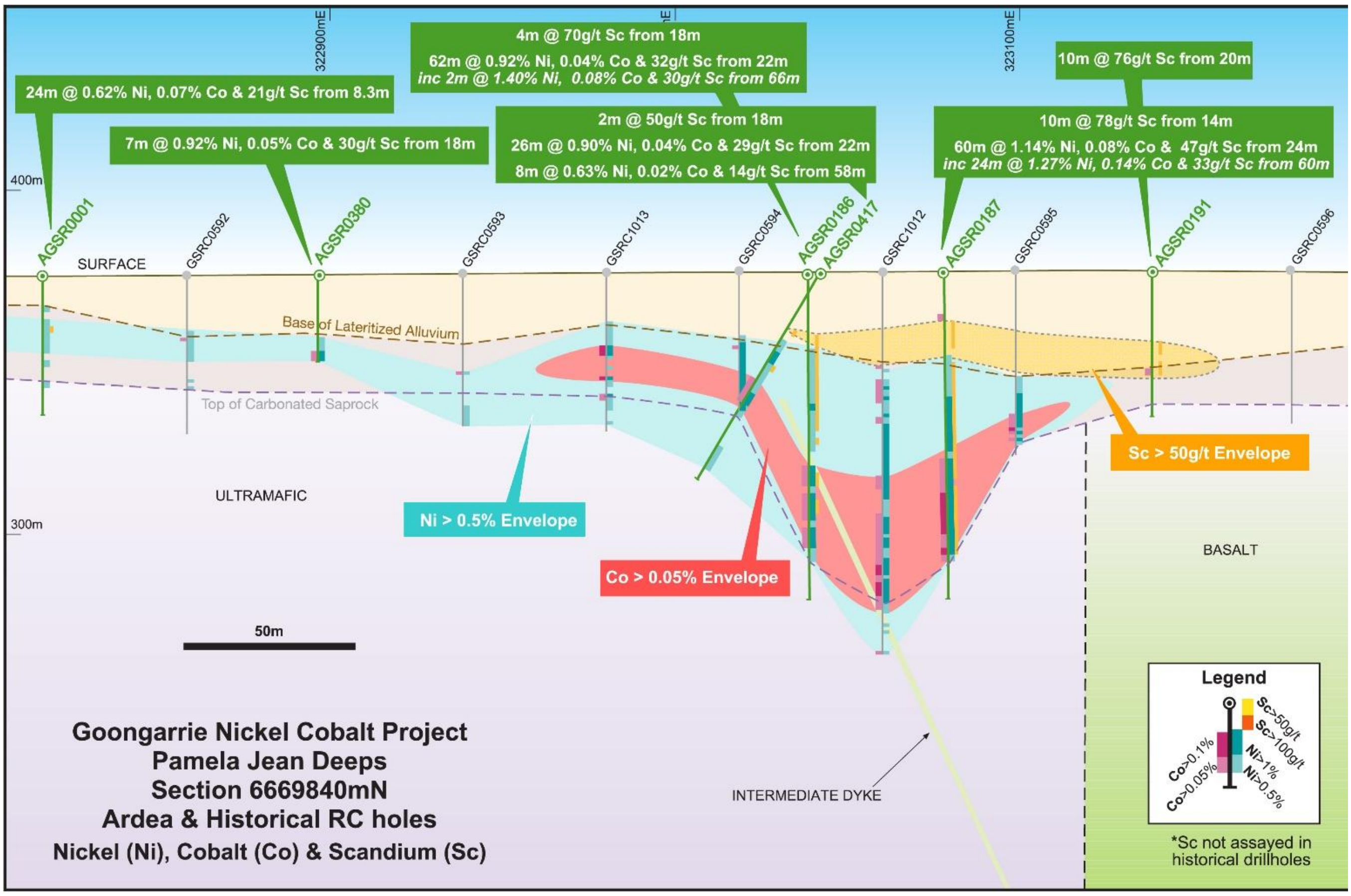
The same bedrock structures also control the location of palaeo-channel quartz sand units (component of "Lateritized Alluvials", Figure 2-9). The sand channels influence DFS hydrology planning and pit designs.

Protolith

The Goongarrie nickel-cobalt mineralization is hosted by the Walter Williams Formation (WWF), a 2.7 billon year old olivine cumulate komatiite volcanic flow. The flow at its western contact variously overlies a granitoid basement or Missouri Basalt (conformable volcanic contact). The upper eastern contact is conformable Siberia Komatiite, with potential for a low-grade nickel laterite regolith.

Western-most Goongarrie drill holes intersect a major quartz sand palaeo-channel aquifer (including carbonate bands), either overlying mineralization or dissecting mineralization. The palaeo-channel is a NW palaeo-valley separating Pamela Jean in the east from Elsie Tynan in the west.

Eastern-most Goongarrie drill holes end in olivine orthocumulate and Siberia Komatiite and have a nontronite regolith with low-grade nickel laterite developed on shallow dolomitic saprock (potential neutralizer).



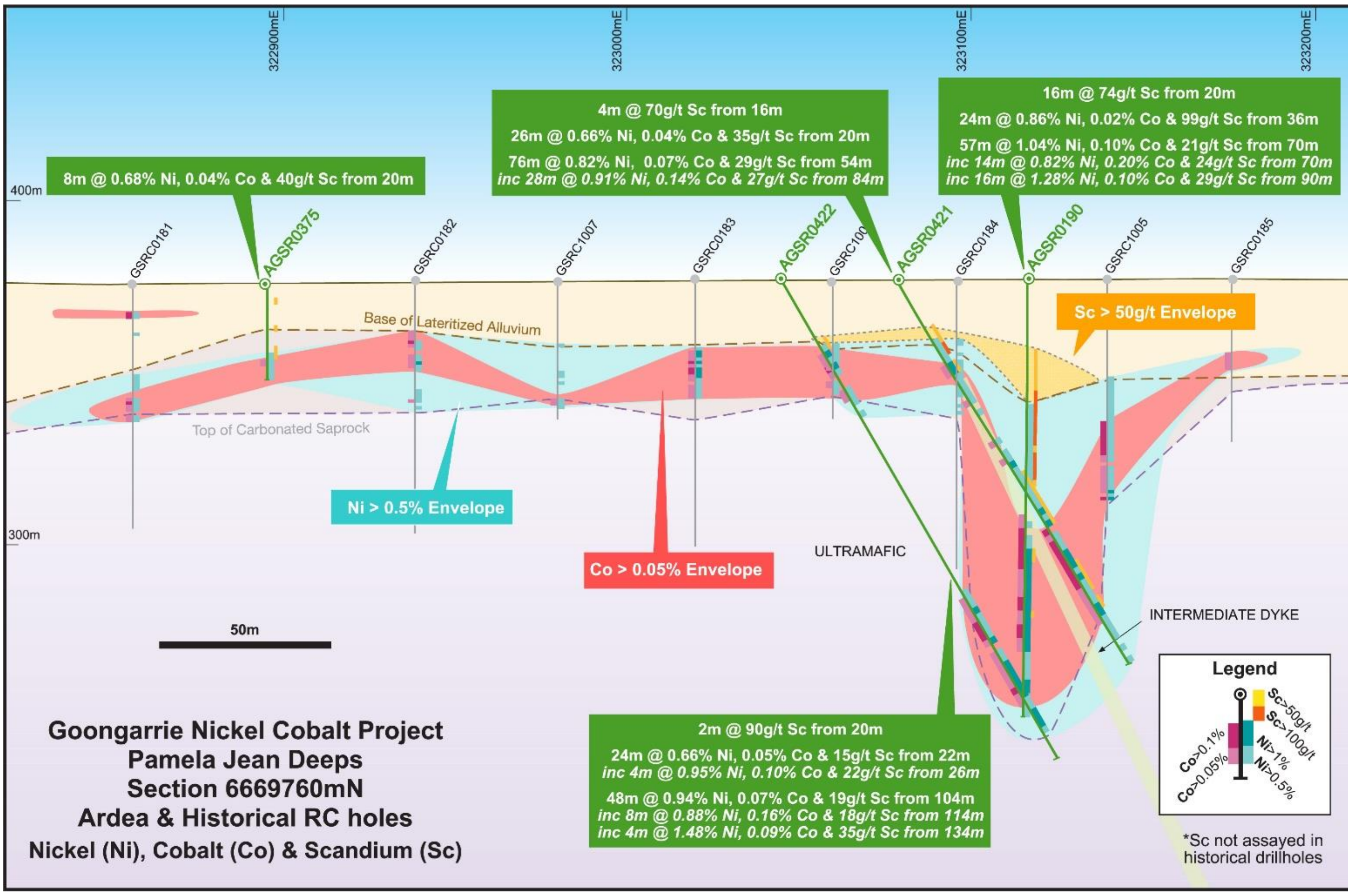


Figure 4 *Section 6669840mN* *Figure 5* *Section 6669760mN*

Regolith

As well as being the ore body, the Regolith is critical to project design, providing civil construction material, and importantly neutralizer for the PAL discharge and environmental management.

The drill-hole logging and interpretation defines the regolith, which then governs mine scheduling for ore, neutralizer and construction materials.

Goongarrie has a predicable Regolith, easily recognized in drill logging and is summarized as follows.

Pedogenic – Regolith Cycle 3 - Residual (youngest)

Modern soil profile, typical detrital quartz sand with colluvial hematitic clasts cemented by calcite at 0-2m and dolomite at 2-6m, commonly colluvial gravel horizons.

The carbonate component is suited as an environmental neutralizer.

Laterite – Regolith Cycle 2 - Residual

Laterite Duricrust is dominantly ferruginous (>25% Fe) and usually develops on Alluvial cover, but on palaeo-Tertiary highs such as Patricia Anne, laterite develops on a mineralized goethite cumulate substrate.

The Laterite Mottled is a distinctive dark red massive mottled kaolinitic clay with Sc-V-Ti-Zr "resistate" enrichment. XRD confirms a haematite-kaolinite mineralogy. There can be a diagnostic alunite overprint superimposed upon upper Cycle 2 Laterite.

Laterite is earmarked for use in civil earthworks, including plant site, ROM pad and roadways.

Alluvial Cover – Regolith Cycle 1, 2 - Depositional

The Alluvial Cover includes Tertiary-aged gravel, sand and clay overburden. For consistency, if ferricrete bands are present (yellow/brown mottling or dark red hematite nodules), then the material characterization is Laterite, and it is suitable for earthworks.

Tertiary palaeo-channel gravels with carbonate cement typically show no lateritization. The magnesite is suitable for neutralization of the PAL discharge, but lacks the nickel credit of saprock neutralizer.

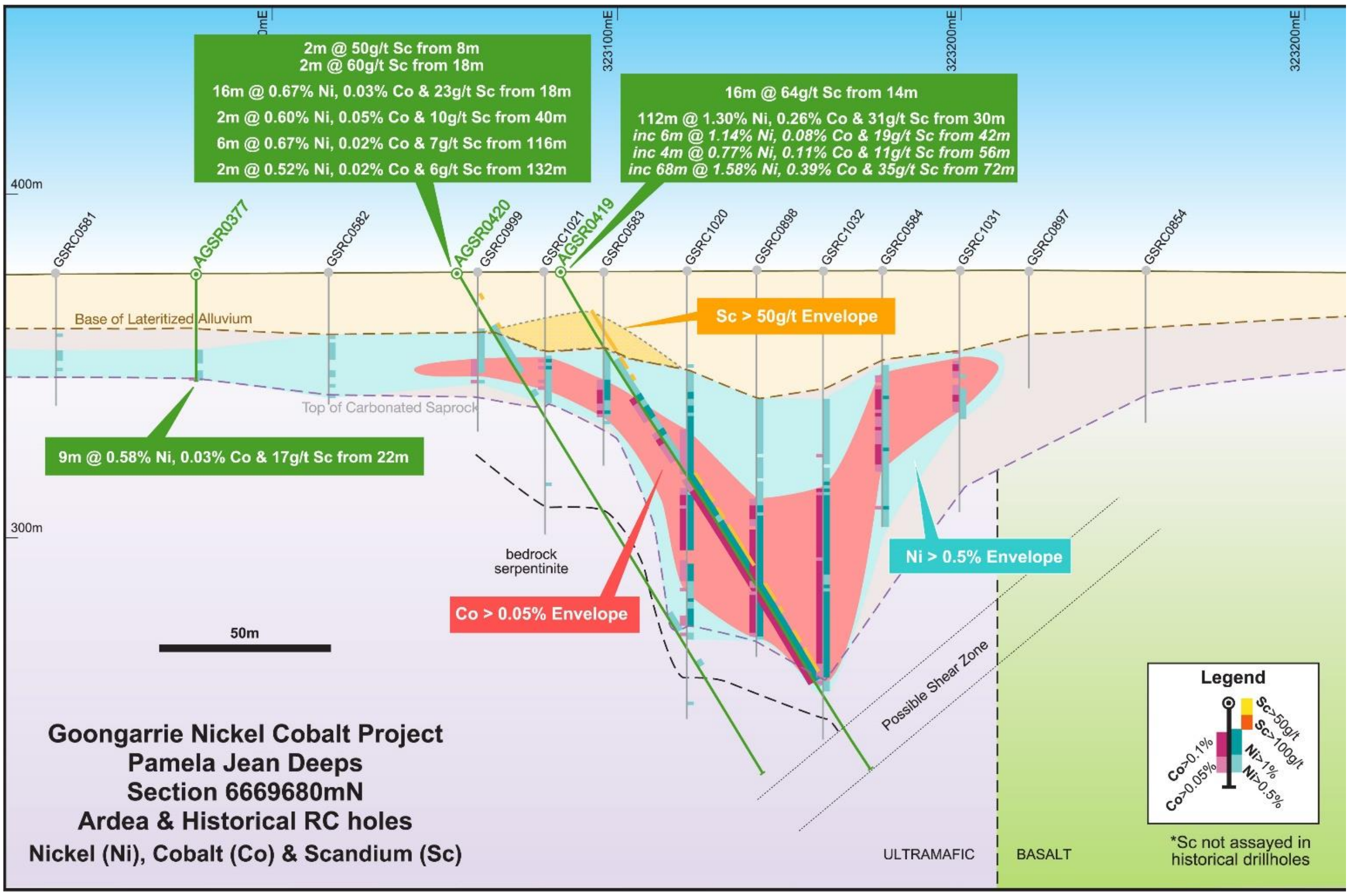
A distinctive clay variant is "candy-stripe clay", being a thin bedded 0.2-2mm banded white and brown-pink kaolinitic lacustrine deposit which has been irregularly "bleached" to pure white (to blue-green-white) coating-grade kaolinite. This is a high priority precursor target for High Purity Alumina (HPA).

Clay Upper – Regolith Cycle 1 - Residual (oldest)

The main mineralized zone at Goongarrie is termed Clay Upper/Lower and occurs dominantly between base of Cycle 2 Lateritized Alluvials and top of Cycle 1 Carbonated Saprock (Figures 2-9).

Clay Upper mineralogy is dominantly goethite clay, with accessory asbolite, haematite, magnetite, chromite, kaolinite, gibbsite and silica. The ore zone in modelling is clearly defined by the >0.5% Ni grade shell, with associated Co, Mn, Cr, Zn and Cl enrichment.

The continuity of Clay Upper/Lower mineralization ensures predictability and accuracy for mine scheduling, significantly diminishing production risk at Goongarrie.



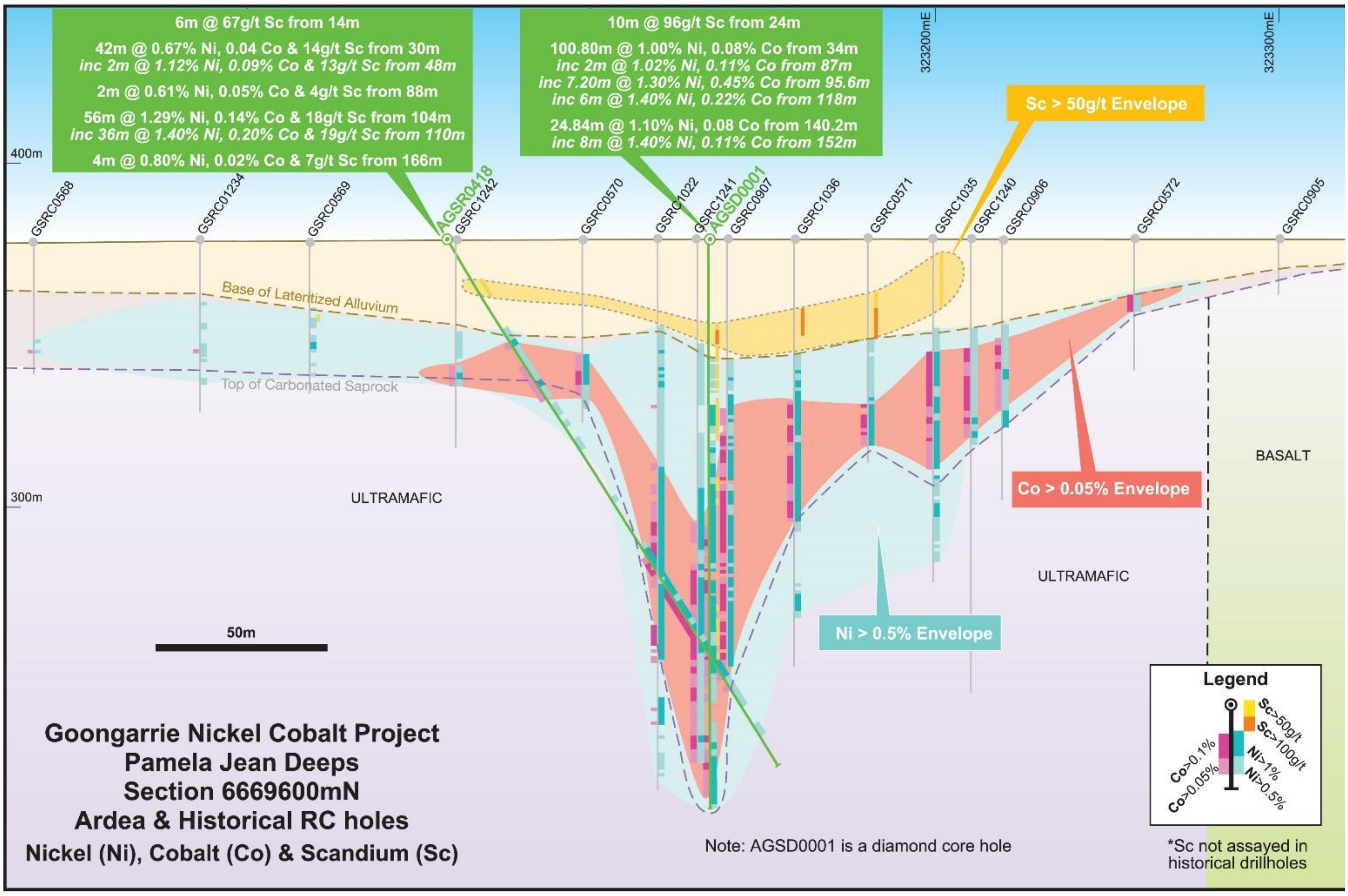


Figure 6 *Section 6669680mN* *Figure 7* *Section 6669600mN*

The base off Clay Upper is a geochemical contact termed the Magnesia Discontinuity (MD), characterized by a sharp increase in magnesium and silica with a corresponding decrease in iron and aluminium which reflects palaeo-water table events. There is a marked increase in Ni, Co and Mn straddling the MD.

Clay Lower – Regolith Cycle 1 - Residual

Clay Lower is the mineralization host below the Magnesia Discontinuity. There is invariably 2-10m of mineralized Clay Lower below the MD and above Saprock. Clay Lower is dominantly goethite, with accessory silica, chlorite-serpentine (green flecks) and magnesite (white-brown).

Clay Void-fill – Regolith Cycle 1 - Residual

Clay Void-fill is a distinctive karst-style breccia deposit occasionally found at the top of Saprock, consisting of irregular angular fragments of silicified Saprock "floating" in a dark red goethitic mud matrix.

The silicified fragments are suited as a grinding media, which is attractive in view of the nickel credit of Clay Void-fill (0.5-1.3% Ni).

Saprock – Regolith Cycle 1 - Residual

Saprock is a hard carbonated weathered rock with strong remnant olivine cumulate textures. It is easily distinguished from the overlying soft ore, so the base of ore will be readily distinguished in grade control. Geochemically, Saprock has >7% Ca and >20% LOI. There is a strong vertical zonation with depth in Saprock, being dolomite to magnesite to silica and finally serpentinite with irregular veining of porcellanous magnesite and chalcedony. At Pamela Jean, the dolomite zone is generally absent.

Saprock is suited as a PAL discharge neutralizer, with the focus on nickel-bearing carbonate (target 0.4-0.8% Ni).

Bedrock - Protolith

Bedrock has only been intersected by Ardea in the Pamela Jean Deeps "batter" geotechnical holes. Previous interpretations at Goongarrie are that olivine adcumulate weathers to deep goethite-gibbsite-silica clays, mesocumulate to shallower nontronite clays and orthocumulate has a very thin carbonated saprock weathering profile.

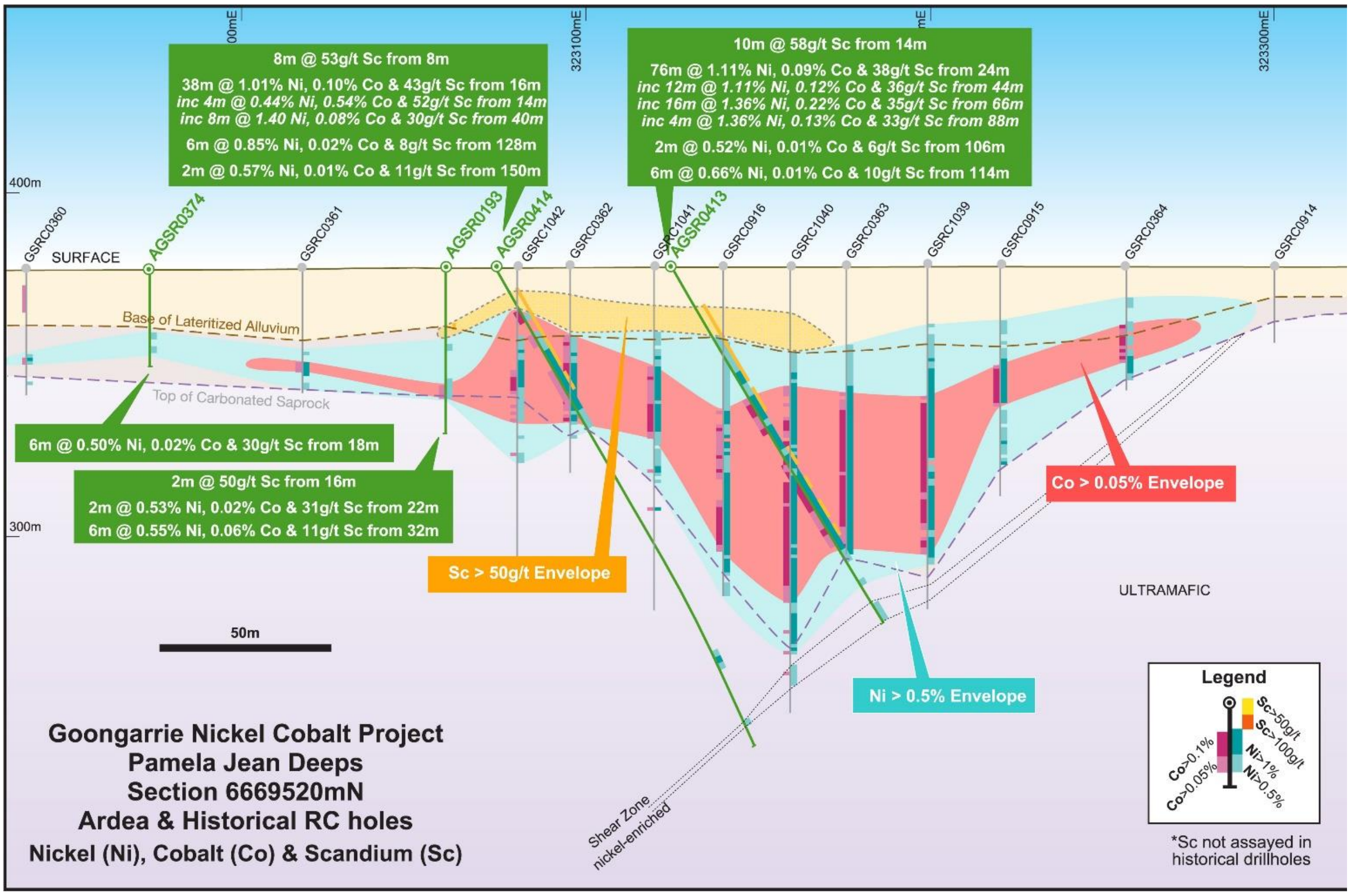
Mineralization

Pamela Jean is the key constituent lateritic orebody that contributes to the ore reserves defined at the Goongarrie Nickel Cobalt Project. It is located at the central Goongarrie South area (Figure 1). It is one of the 31 currently defined deposits modelled for future mining at Goongarrie (see Appendix 1).

The Pamela Jean deposit measures approximately 1,700 metres by 300 metres and is characterised by high-grade, "deep funnel"-shaped mineralization. Overburden is 20-30m, with base of Pamela Jean Deeps mineralization between 100 and 165m.

The top of Pamela Jean is a typical flat laterite surface at 15-30m below surface. Rather than a flat base some 40-50m below surface, the base of Pamela Jean is concave at 80-165m below surface forming a "funnel-shaped" ore geometry that fortuitously mimics pit design batters, so minimizing Pamela Jean strip ratios. The result is high tonnes and grade proximal to the future plant site.

Continuity of mineralization is strong between drill holes (Figure 2-9). This is a hallmark of Goongarrie, being a "goethite style" (yellow) laterite nickel-cobalt deposit. It contrasts with the more siliceous and nontronitic style (green) laterite deposits which can exhibit marked variation between drill-holes. All defined intercepts from the 2018 Pamela Jean program are listed in Appendix 3.



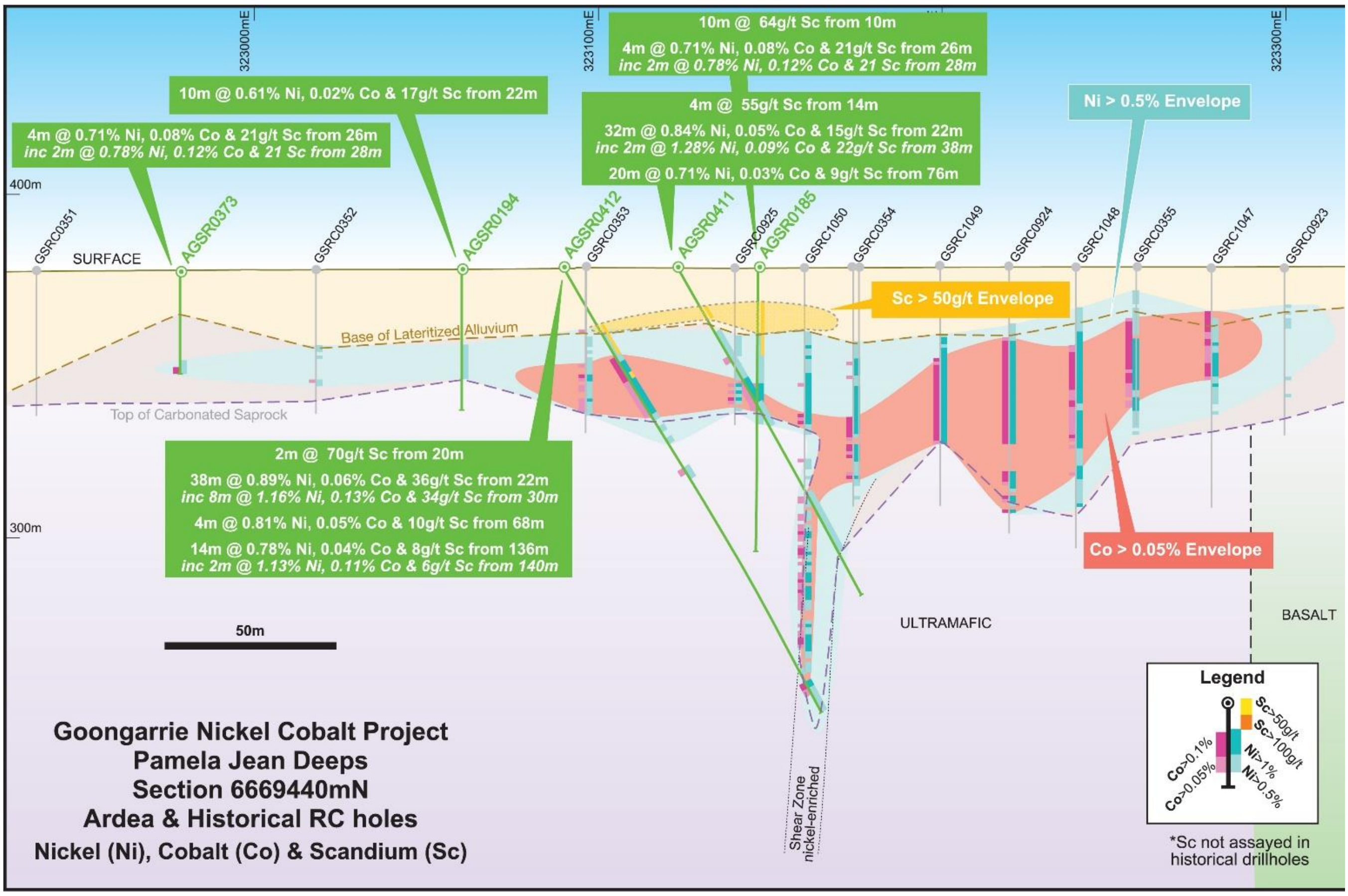


Figure 8 *Section 6669520mN* *Figure 9* *Section 6669440mN*

Metallurgical Programs

The 2018 Pamela Jean drilling has been a key source of metallurgical test material for current DFS programs.

Variability studies

Representative "run-of-mine" mineralization from Ardea Goongarrie South diamond core holes AGSD0007, 0010 and 0012 was used in the study. The consistency of mineralization has been confirmed and final results are pending.

Piloting studies

Based on the optimized pit schedule material, pilot feed was specifically-drilled with sonic core at 200m intervals along the strike of Pamela Jean and Elsie Tynan pit areas and supplemented with bulk RC chips from the Patricia Anne pit area, to achieve an approximate 1.1% Ni, 0.12% Co and 35g/t Sc feed (7.5 tonne dry).

The dominant ore style at Goongarrie is goethite-rich, with an accessory cobaltian wad termed asbolite. The ore has exceptional rheology in terms of pulp density and settling, with very consistent metallurgical performance.

Leaching has been completed to produce Mixed Sulphide Product (MSP). Metal leach extractions were 93-95%. The MSP is currently being refined into sulphate crystals. This process should be complete by the end of October 2018.

Ongoing work at Goongarrie

Resource Estimation

A comprehensive resource re-estimation for Goongarrie commenced in July 2018 in the northern Goongarrie project area (Patricia Anne) whilst drilling was still current in the southern project area (Big Four, Scotia Dam). The resource re-estimation due this quarter and will incorporate the recent infill drilling at Elsie Tynan.

During the course of wireframing the Patricia Anne and Pamela Jean deposits and siting geotechnical holes, it became apparent that though the 80x40m drill pattern was more than adequate for the run-of-mine "shallow flat" ore that typically occurs between 20m and 40m vertical depth, there were limitations for deeper ore. With the recognition of the strong structural controls on "deep funnel" ore, it became apparent that the 80x40m pattern did not adequately quantify the "deep funnel" ore with a large number of previous holes being stopped in ore (due to failing to identify the deep structural control on mineralization).

These observations indicate a resource predicated on existing drilling could underestimate the contribution of these "funnels".

An indicator of this issue was the pilot plant deep sonic drilling in most holes returned ore that significantly exceeded predicted the "run-of-mine" grades of 1% Ni and 0.1% Co, necessitating low grade hanging wall ore to be included in piloting to return grade closer to the scheduled life-of-mine grades.

Geo-metallurgy

Detailed geo-metallurgical analysis is currently underway for Goongarrie using multi-element geochemistry and Xray Diffraction (XRD) mineralogical analysis.

The study will allow 2018 Ardea drilling to be used as a control to populate the historic data base in respect of predicted metallurgical performance and material characterization.

There are currently 10 variants of Clay Upper ore and 8 variants of Clay Lower ore, all requiring variability test work.

The geo-metallurgical work on 28 Ardea core holes suggests the bulk density of "run-of-mine" ore historically may have been over-estimated, implying a potential reduction in tonnage but the historic bulk density determination estimates far exceed the smaller Ardea bulk density data set.

Drilling programs

A limited program of 80x20m infill RC drilling is under consideration for late 2018 to better quantify the "deep funnel" targets. This would enable an upgrade of resources and reserves, so facilitating greater confidence in defining mining schedules for the planned Goongarrie mine.

Additional drilling also includes:

- Ongoing samples for metallurgical variability testing of mineralized zones.
- Hydrology, palaeo-channel quartz sands separate the various ore bodies, so require pump-testing.
- Geotechnical, recent drill-hole AGSR0420 was a "sighter hole" for geotechnical core drilling. AGSR0420 intersected saprock and bedrock as predicted by Ardea's pre-drill wireframe, with RC chip logging suggesting a hard, competent rock suited to pit batter positioning.

DFS optimization options

The March 2018 Pre-Feasibility Study and July 2018 Expansion Study for the Goongarrie Nickel Cobalt Project highlighted an exceptional business case. With an enormous KNP resource inventory, access to discrete high-grade cobalt zones ("deep funnels") and the 2018 scandium and neutraliser discoveries, further project upside is expected at Goongarrie with studies underway for:

- Potential to high-grade the mining of cobalt zones during payback period, due to more constrained sub-blocking the resource model (smaller selective blocks in the updated resource model).
- Increased throughput and production through multiple (2.25Mtpa) PAL trains.
- Scandium production.
- Mineralized neutraliser optimization.

Other possibilities to further enhance the project that are under consideration involve monetising accessory metals including vanadium, battery-grade manganese, high-purity alumina and chromium.

For further information regarding Ardea, please visit www.ardearesources.com.au or contact:

Ardea Resources:
Ms Katina Law
Executive Chair, Ardea Resources Limited
Tel +61 8 6244 5136

Compliance Statement (JORC 2012)

A competent person's statement for the purposes of Listing Rule 5.22 has previously been announced by the Company for:

1. *Kalgoorlie Nickel Project on 21 October 2013 and 31 June 2014, October 2016, 2016 Heron Resources Annual Report and 6 January 2017;*
2. *KNP Cobalt Zone Study on 6 January 2017*

The Company confirms that it is not aware of any new information or data that materially affects information included in previous announcements, and all material assumptions and technical parameters underpinning the estimates continue to apply and have not materially changed. All projects will be subject to new work programs following the listing of Ardea, notably drilling, metallurgy and JORC Code 2012 resource estimation as applicable.

The information in this report that relates to KNP Exploration Results is based on information originally compiled by previous and current full time employees of Heron Resources Limited and after February 2017 employees of Ardea Resource Limited. The Exploration Results and data collection processes have been reviewed, verified and re-interpreted by Mr Ian Buchhorn who is a Member of the Australasian Institute of Mining and Metallurgy and currently a director of Ardea Resources Limited. Mr Buchhorn has sufficient experience that is relevant to the style of mineralization and type of deposit under consideration and to the exploration activities undertaken to qualify as a Competent Person as defined in the 2012 Edition of the 'Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves'. Mr Buchhorn consents to the inclusion in this report of the matters based on his information in the form and context that it appears.

The exploration and industry benchmarking summaries are based on information reviewed by Dr Matthew Painter, who is a Member of the Australian Institute of Geoscientists. Dr Painter is a full-time employee and a director of Ardea Resources Limited and has sufficient experience, which is relevant to the style of mineralization and type of deposit under consideration and to the activity which he is undertaking to qualify as a Competent Person as defined in the 2012 edition of the Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves'. Mr Buchhorn and Dr Painter has reviewed this press release and consents to the inclusion in this report of the information in the form and context in which it appears.

CAUTIONARY NOTE REGARDING FORWARD-LOOKING INFORMATION

This news release contains forward-looking statements and forward-looking information within the meaning of applicable Australian securities laws, which are based on expectations, estimates and projections as of the date of this news release.

This forward-looking information includes, or may be based upon, without limitation, estimates, forecasts and statements as to management's expectations with respect to, among other things, the timing and ability to complete the Ardea spin-out, the timing and amount of funding required to execute the Company's exploration, development and business plans, capital and exploration expenditures, the effect on the Company of any changes to existing legislation or policy, government regulation of mining operations, the length of time required to obtain permits, certifications and approvals, the success of exploration, development and mining activities, the geology of the Company's properties, environmental risks, the availability of labour, the focus of the Company in the future, demand and market outlook for precious metals and the prices thereof, progress in development of mineral properties, the Company's ability to raise funding privately or on a public market in the future, the Company's future growth, results of operations, performance, and business prospects and opportunities. Wherever possible, words such as "anticipate", "believe", "expect", "intend", "may" and similar expressions have been used to identify such forward-looking information. Forward-looking information is based on the opinions and estimates of management at the date the information is given, and on information available to management at such time. Forward-looking information involves significant risks, uncertainties, assumptions and other factors that could cause actual results, performance or achievements to differ materially from the results discussed or implied in the forward-looking information. These factors, including, but not limited to, the ability to complete the Ardea spin-out on the basis of the proposed terms and timing or at all, fluctuations in currency markets, fluctuations in commodity prices, the ability of the Company to access sufficient capital on favourable terms or at all, changes in national and local government legislation, taxation, controls, regulations, political or economic developments in Australia or other countries in which the Company does business or may carry on business in the future, operational or technical difficulties in connection with exploration or development activities, employee relations, the speculative nature of mineral exploration and development, obtaining necessary licenses and permits, diminishing quantities and grades of mineral reserves, contests over title to properties, especially title to undeveloped properties, the inherent risks involved in the exploration and development of mineral properties, the uncertainties involved in interpreting drill results and other geological data, environmental hazards, industrial accidents, unusual or unexpected formations, pressures, cave-ins and flooding, limitations of insurance coverage and the possibility of project cost overruns or unanticipated costs and expenses, and should be considered carefully. Many of these uncertainties and contingencies can affect the Company's actual results and could cause actual results to differ materially from those expressed or implied in any forward-looking statements made by, or on behalf of, the Company. Prospective investors should not place undue reliance on any forward-looking information.

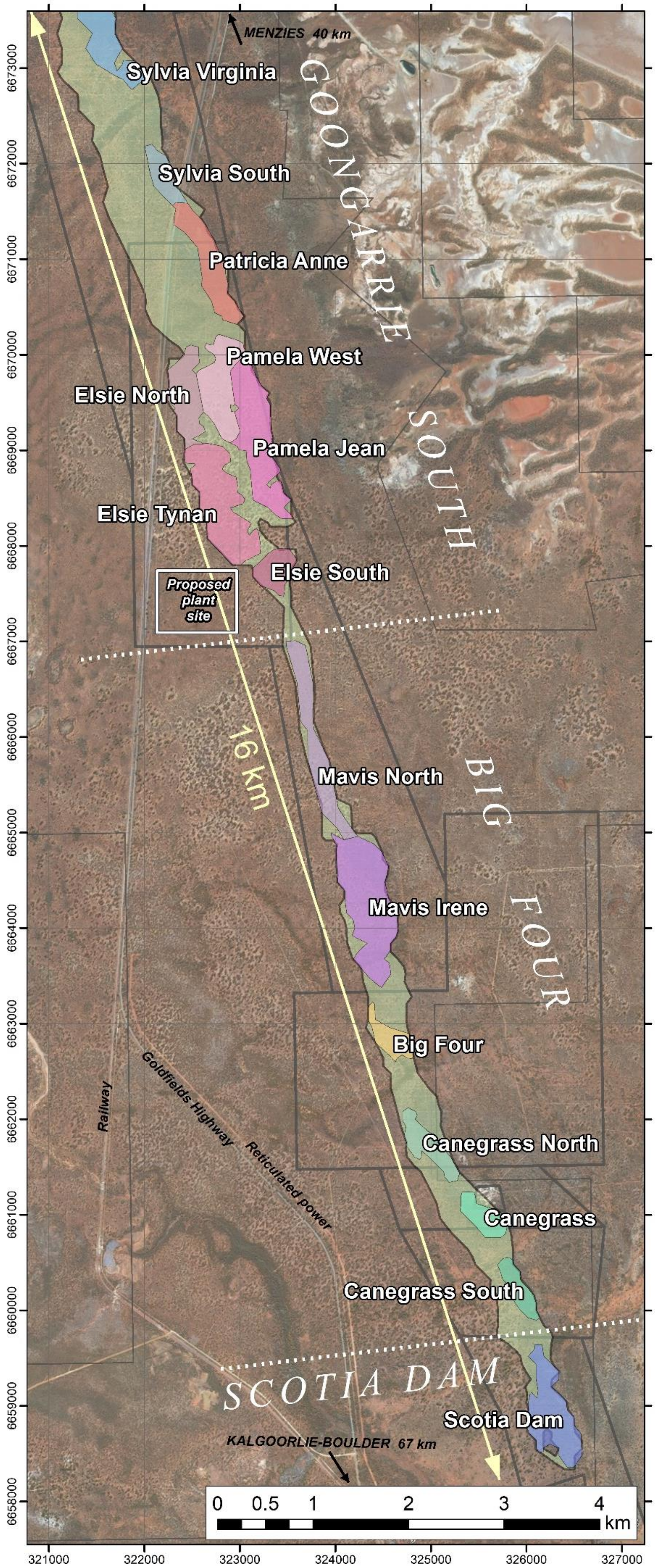
Although the forward-looking information contained in this news release is based upon what management believes, or believed at the time, to be reasonable assumptions, the Company cannot assure prospective purchasers that actual results will be consistent with such forward-looking information, as there may be other factors that cause results not to be as anticipated, estimated or intended, and neither the Company nor any other person assumes responsibility for the accuracy and completeness of any such forward-looking information. The Company does not undertake, and assumes no obligation, to update or revise any such forward-looking statements or forward-looking information contained herein to reflect new events or circumstances, except as may be required by law.

No stock exchange, regulation services provider, securities commission or other regulatory authority has approved or disapproved the information contained in this news release.

Appendix 1 – Constituent deposits and orebodies of the Goongarrie Nickel Cobalt Project

Deposits of the Goongarrie Nickel Cobalt Project, from Sylvia Virginia in the north to Scotia Dam in the south, a distance of 16km. Active mining tenements are outlined in black.

Deposits are marked by significant nickel and cobalt mineralization and are encased within the overall nickel envelope (green, Ni>0.5%).



Appendix 2 – Pit schedule diagram for Goongarrie South

Pit scheduling identifies Patricia Anne for the first two pits of the Goongarrie Nickel Cobalt Project.

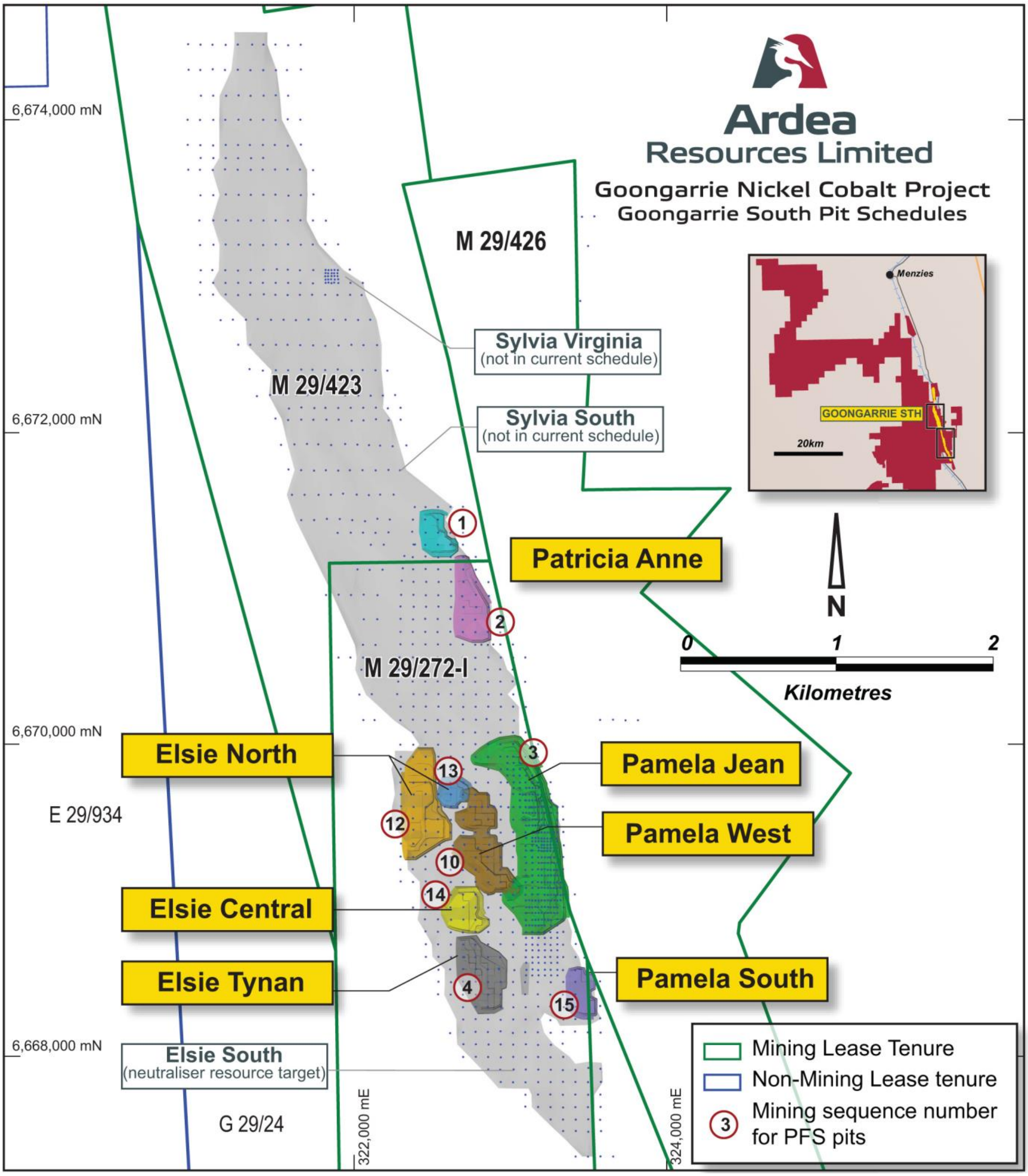


Figure 2 – Pit schedules for the Goongarrie South part of the Goongarrie Nickel Cobalt Project

Appendix 3 – Collar location data

Drill holes by Ardea Resources at Pamela Jean Deeps

Drill hole	Type	Depth (m)	Tenement	Grid	Easting (mE)	Northing (mN)	RL (mASL)	Dip (°)	Azimuth (°)
AGSD0001	DD	165.3	M29/00272	MGA94_51	323134	6669598	378	-90	000
AGSR0001	RC	40.3	M29/00272	MGA94_51	322816	6669840	375	-90	000
AGSR0185	RC	83	M29/00272	MGA94_51	323146	6669442	379	-90	000
AGSR0186	RC	95	M29/00272	MGA94_51	323039	6669839	376	-90	000
AGSR0187	RC	95	M29/00272	MGA94_51	323078	6669842	376	-90	000
AGSR0190	RC	127	M29/00272	MGA94_51	323116	6669760	377	-90	000
AGSR0191	RC	42	M29/00272	MGA94_51	323139	6669837	376	-90	000
AGSR0193	RC	48	M29/00272	MGA94_51	323059	6669517	378	-90	000
AGSR0194	RC	41	M29/00272	MGA94_51	323060	6669441	378	-90	000
AGSR0291	RC	31	M29/00272	MGA94_51	323140	6669880	376	-90	000
AGSR0292	RC	30	M29/00272	MGA94_51	323181	6669881	376	-90	000
AGSR0293	RC	35	M29/00272	MGA94_51	323138	6669923	376	-90	000
AGSR0294	RC	51	M29/00272	MGA94_51	322897	6669922	375	-90	000
AGSR0295	RC	53	M29/00272	MGA94_51	322818	6669925	375	-90	000
AGSR0373	RC	30	M29/00272	MGA94_51	322978	6669437	378	-90	000
AGSR0374	RC	28	M29/00272	MGA94_51	322973	6669517	377	-90	000
AGSR0375	RC	28	M29/00272	MGA94_51	322895	6669757	376	-90	000
AGSR0377	RC	31	M29/00272	MGA94_51	322978	6669689	377	-90	000
AGSR0380	RC	25	M29/00272	MGA94_51	322896	6669837	375	-90	000
AGSR0411	RC	110	M29/00272	MGA94_51	323123	6669441	379	-60	100
AGSR0412	RC	150	M29/00272	MGA94_51	323090	6669432	379	-60	100
AGSR0413	RC	120	M29/00272	MGA94_51	323125	6669513	378	-60	100
AGSR0414	RC	158	M29/00272	MGA94_51	323074	6669511	378	-60	090
AGSR0415	RC	80	M29/00272	MGA94_51	323038	6669921	375	-90	000
AGSR0416	RC	90	M29/00272	MGA94_51	323038	6669875	376	-90	000
AGSR0417	RC	70	M29/00272	MGA94_51	323042	6669834	376	-60	270
AGSR0418	RC	180	M29/00272	MGA94_51	323059	6669592	377	-60	090
AGSR0419	RC	170	M29/00272	MGA94_51	323083	6669684	377	-60	090
AGSR0420	RC	170	M29/00272	MGA94_51	323054	6669685	377	-60	090
AGSR0421	RC	130	M29/00272	MGA94_51	323078	6669748	377	-60	090
AGSR0422	RC	160	M29/00272	MGA94_51	323045	6669748	377	-60	090

Appendix 4 – Assay results from Pamela Jean Deeps

All assays from recent drilling at Pamela Jean Deeps, Goongarrie South.

Abbreviations used: Co – cobalt, Ni – nickel, Sc – scandium, Mn – Manganese, Cr – chromium, V – vanadium, Au – gold, m – metre, g/t – grams per tonne, ppm – parts per million, ppb – parts per billion, bd – below detection.

Hole	From (m)	To (m)	Sample number	Ni (%)	Co (%)	Sc (g/t)	Mn (ppm)	Cr (ppm)	V (ppm)	Au (ppb)
AGSD0001	1.9	4	S200841	0.016	bd	bd	186	732	123	8
AGSD0001	4	6	S200842	0.02	bd	10	101	2052	224	3
AGSD0001	6	8	S200843	0.024	bd	10	70	2873	342	3
AGSD0001	8	10	S200844	0.034	0.001	30	62	2825	196	1
AGSD0001	10	12	S200845	0.029	bd	30	70	1936	151	2
AGSD0001	12	14	S200846	0.031	0.002	30	62	2031	134	3
AGSD0001	14	16	S200847	0.031	0.001	10	116	3618	291	2
AGSD0001	16	18	S200848	0.021	0.002	20	178	5219	426	2
AGSD0001	18	20	S200849	0.031	0.002	20	147	6573	515	2
AGSD0001	20	21.9	S200851	0.055	0.006	30	178	9371	762	2
AGSD0001	22.6	24.3	S200852	0.09	0.006	20	209	10876	739	1
AGSD0001	24.3	26.2	S200853	0.19	0.012	70	194	16826	941	4
AGSD0001	26.2	28.2	S200854	0.295	0.012	120	248	15185	403	5
AGSD0001	28.2	30.3	S200855	0.346	0.012	130	271	16005	258	3
AGSD0001	30.3	32	S200856	0.494	0.017	90	387	9234	202	5
AGSD0001	32	34	S200857	0.439	0.019	70	457	9166	123	3
AGSD0001	34	35.57	S200858	0.574	0.018	70	945	8824	252	4
AGSD0001	36.07	38.5	S200859	0.565	0.014	50	960	7387	235	2
AGSD0001	38.5	40.4	S200862	0.821	0.017	50	643	12722	213	bd
AGSD0001	40.8	43.1	S200863	0.798	0.021	60	837	13748	230	2
AGSD0001	43.8	44.5	S200864	0.527	0.011	60	713	11081	241	4
AGSD0001	44.5	46	S200865	0.259	0.006	40	527	13064	319	2
AGSD0001	46	48	S200866	0.383	0.013	50	968	13475	303	2
AGSD0001	48	50.2	S200867	1.12	0.016	60	1038	24829	190	bd
AGSD0001	50.2	52.1	S200868	1.495	0.028	60	1665	33858	168	1
AGSD0001	52.1	54	S200869	1.165	0.025	50	1596	32148	157	2
AGSD0001	54	56.3	S200871	0.533	0.026	50	1596	33584	196	1
AGSD0001	56.3	58.4	S200872	0.287	0.028	60	930	20930	213	1
AGSD0001	58.4	59.9	S200873	0.919	0.017	40	1658	16005	146	bd
AGSD0001	60.3	62	S200874	1.04	0.021	30	1774	17784	118	bd
AGSD0001	62	63	S200875	0.76	0.013	30	1425	15800	106	bd
AGSD0001	63	65	S200876	0.959	0.023	30	1936	22161	118	4
AGSD0001	65	67	S200877	1.445	0.028	30	2432	22435	140	2
AGSD0001	67	69	S200878	1.275	0.042	30	2742	19289	168	bd
AGSD0001	69	71	S200879	0.971	0.034	50	2022	19699	207	1
AGSD0001	71	73	S200881	1.155	0.038	50	1967	15800	185	2
AGSD0001	73	75	S200882	1.23	0.043	30	1936	14364	134	1
AGSD0001	75	77	S200883	1.335	0.045	60	2076	14911	179	bd
AGSD0001	77	79	S200884	1.055	0.04	30	1642	12893	129	2
AGSD0001	79	81	S200885	1.055	0.048	40	1658	9986	151	2
AGSD0001	81	83	S200886	1.09	0.048	20	1712	11047	146	1
AGSD0001	83	85	S200887	1.005	0.057	20	1960	10602	140	2
AGSD0001	85	87	S200888	1.255	0.057	30	1588	11560	157	2
AGSD0001	87	89	S200889	1.02	0.112	20	2579	9815	118	107
AGSD0001	89	91	S200891	1.255	0.057	10	1317	10226	78	5
AGSD0001	91	92	S200892	1.085	0.037	10	705	10773	84	12
AGSD0001	92	94	S200893	1.21	0.058	20	1224	11149	50	34
AGSD0001	94	95.6	S200894	0.963	0.039	20	1015	12449	84	45
AGSD0001	95.6	96.4	S200895	3.16	1.95	20	139427	12038	50	6
AGSD0001	98.9	100	S200896	2.14	0.897	30	36406	27975	123	2
AGSD0001	100	101	S200897	1.75	0.319	30	11774	23803	123	4
AGSD0001	101	102.8	S200898	1.495	0.213	30	6979	21888	101	2
AGSD0001	103.4	106	S200901	1.18	0.061	40	1805	33653	179	30
AGSD0001	106.2	108	S200902	1.295	0.068	60	1317	41245	207	20
AGSD0001	108	110	S200903	1.29	0.055	40	1317	33926	190	17
AGSD0001	110	112	S200904	1.22	0.064	60	1611	39261	202	51
AGSD0001	112	114	S200905	1.005	0.05	50	1216	29822	190	1
AGSD0001	114	116	S200906	0.775	0.05	60	1363	44665	263	2
AGSD0001	116	118	S200907	0.821	0.046	60	1317	31943	246	6
AGSD0001	118	120	S200908	1.57	0.41	40	12820	27155	202	41
AGSD0001	120	122	S200909	1.53	0.163	50	7072	33789	179	44
AGSD0001	122	124	S200911	1.11	0.099	30	7273	25581	146	1
AGSD0001	124	126	S200912	1.295	0.078	40	3470	29001	162	9
AGSD0001	126	127.3	S200913	0.967	0.052	40	976	23393	118	4
AGSD0001	127.7	130	S200914	0.904	0.053	40	960	21341	129	5
AGSD0001	130	132	S200915	0.667	0.041	20	875	17989	73	1
AGSD0001	132	134.1	S200916	0.896	0.068	20	1991	11833	84	5
AGSD0001	134.3	134.8	S200917	0.916	0.022	20	930	10499	78	bd
AGSD0001	135.3	137	S200918	0.467	0.025	10	1208	4617	39	bd
AGSD0001	137	139	S200919	0.212	0.012	10	991	4378	22	1
AGSD0001	139	140.2	S200921	0.346	0.024	bd	1332	4405	22	3
AGSD0001	140.2	142.3	S200922	0.761	0.049	10	2696	7353	50	3
AGSD0001	142.5	144.1	S200923	0.659	0.045	20	1146	8140	73	bd
AGSD0001	144.1	146	S200924	0.841	0.169	10	6321	10499	50	1
AGSD0001	146	148	S200925	1.01	0.046	10	3400	12209	50	5
AGSD0001	148	150	S200926	0.798	0.059	20	1727	9302	67	bd
AGSD0001	150	152	S200927	1.275	0.064	20	1913	17100	73	6
AGSD0001	152	154	S200928	1.34	0.194	20	13633	13167	28	36
AGSD0001	154	156	S200929	1.03	0.083	20	6917	11525	45	bd
AGSD0001	156	158	S200931	1.32	0.064	40	5019	14501	118	5
AGSD0001	158	160	S200932	1.915	0.094	30	8869	27907	140	1
AGSD0001	160	162	S200933	1.445	0.053	30	5964	19836	101	8
AGSD0001	162	164	S200934	1.045	0.029	20	3238	17373	78	47
AGSD0001	164	165.04	S200935	0.583	0.03	10	550	8516	50	9
AGSR0001	0	2.3	AR000001	0.021	0.001	12	450	410	100	12
AGSR0001	2.3	4.3	AR000002	0.079	0.016	24	500	1340	200	4
AGSR0001	4.3	6.3	AR000003	0.064	0.007	30	290	2130	400	2
AGSR0001	6.3	8.3	AR000004	0.155	0.018	37	2810	3080	400	bd
AGSR0001	8.3	10.3	AR000005	0.706	0.041	42	1960	3230	100	21
AGSR0001	10.3	12.3	AR000006	0.468	0.024	21	670	3560	100	1
AGSR0001	12.3	14.3	AR000007	0.757	0.046	33	990	3340	bd	3
AGSR0001	14.3	16.3	AR000009	0.815	0.08	49	1680	3660	100	2
AGSR0001	16.3	18.3	AR000010	0.886	0.338	38	18000	3150	200	4
AGSR0001	18.3	20.3	AR000011	0.754	0.077	21	3110	4010	bd	10
AGSR0001	20.3	22.3	AR000012	0.639	0.038	15	1800	2470	bd	3
AGSR0001	22.3	24.3	AR000013	0.426	0.027	9	750	1850	bd	10
AGSR0001	24.3	26.3	AR000014	0.502	0.037	6	2690	1860	bd	3
AGSR0001	26.3	28.3	AR000015	0.459	0.038	7	2000	1930	bd	2
AGSR0001	28.3	30.3	AR000016	0.334	0.028	6	1690	1450	bd	4
AGSR0001	30.3	32.3	AR000017	0.645	0.073	7	4980	2180	bd	3
AGSR0001	32.3	34.3	AR000019	0.343	0.037	4	3970	865	bd	2
AGSR0001	34.3	36.3	AR000020	0.319	0.018	3	1900	680	bd	2
AGSR0001	36.3	38.3	AR000021	0.291	0.011	3	1020	555	bd	1
AGSR0001	38.3	40.3	AR000022	0.222	0.007	3	640	610	bd	bd
AGSR0185	0	2	AR007752	0.014	0.002	8	150	325	bd	17
AGSR0185	2	4	AR007753	0.028	0.001	21	120	3370	400	5
AGSR0185	4	6	AR007754	0.022	bd	14	100	4110	400	2
AGSR0185	6	8	AR007755	0.026	0.001	20	120	4350	400	4
AGSR0185	8	10	AR007757	0.025	0.001	28	120	4730	400	6
AGSR0185	10	12	AR007758	0.109	0.002	33	230	9890	400	1
AGSR0185	12	14	AR007759	0.178	0.005	43	260	13500	300	bd
AGSR0185	14	16	AR007760	0.291	0.006	55	300	15700	100	2
AGSR0185	16	18	AR007761	0.323	0.007	63	260	15200	200	5
AGSR0185	18	20	AR007762	0.432	0.01	64	330	11500	100	4
AGSR0185	20	22	AR007763	0.634	0.022	45	690	6700	100	5
AGSR0185	22	24	AR007764	0.645	0.032	36	690	8230	100	2
AGSR0185	24	26	AR007765	0.601	0.029	39	510	9780	bd	3
AGSR0185	26	28	AR007767	0.757	0.026	27	530	6250	bd	3
AGSR0185	28	30	AR007768	0.68	0.023	25	510	5820	bd	4
AGSR0185	30	32	AR007769	0.661	0.022	20	450	4390	bd	5
AGSR0185	32	34	AR007770	0.975	0.035	24	720	6810	bd	2
AGSR0185	34	36	AR007771	1.09	0.054	20	1220	5600	bd	3
AGSR0185	36	38	AR007772	1.04	0.071	20	2630	5780	bd	3
AGSR0185	38	40	AR007773	1.11	0.192	16	8580	4520	bd	2
AGSR0185	40	42	AR007774	1.06	0.095	11	5280	3210	bd	bd
AGSR0185	42	44	AR007775	0.633	0.039	14	2170	3120	bd	4
AGSR0185	44	46	AR007777	0.556	0.025	8	1880	2370	bd	3
AGSR0185	46	48	AR007778	0.383	0.015	6	1100	1570	bd	3
AGSR0185	48	50	AR007779	0.348	0.015	4	1440	1160	bd	6
AGSR0185	50	52	AR007780	0.269	0.007	4	690	2140	bd	57
AGSR0185	52	54	AR007781	0.221	0.006	4	690	990	bd	6
AGSR0185	54	56	AR007782	0.222	0.008	5	690	1180	bd	4
AGSR0185	56	58	AR007783	0.254	0.01	6	860	1390	bd	3
AGSR0185	58	60	AR007784	0.28	0.011	6	890	1510	bd	1
AGSR0185	60	62	AR007785	0.272	0.01	5	830	1420	bd	2
AGSR0185	62	64	AR007787	0.251	0.01	5	880	1300	bd	2
AGSR0185	64	66	AR007788	0.255	0.01	4	840	1290	bd	bd
AGSR0185	66	68	AR007789	0.218	0.008	5	820	1010	bd	2
AGSR0185	68	70	AR007790	0.248	0.009	5	860	1310	bd	4
AGSR0185	70	72	AR007791	0.253	0.009	5	860	1220	bd	bd
AGSR0185	72	74	AR007792	0.261	0.01	5	840	1350	bd	2
AGSR0185	74	76	AR007793	0.232	0.01	4	780	1240	bd	2
AGSR0185	76	78	AR007794	0.247	0.01	3	800	1460	bd	3
AGSR0185	78	80	AR007795	0.262	0.01	5	820	2350	bd	4
AGSR0185	80	82	AR007797	0.26	0.011	5	920	1870	bd	2
AGSR0185	82	83	AR007798	0.277	0.012	7	880	2330	bd	3
AGSR0186	0	2	AR007799	0.041	0.004	12	290	535	100	28
AGSR0186	2	4	AR007800	0.093	0.005	17	340	1360	100	6
AGSR0186	4	6	AR007801	0.022	0.002	22	140	2200	400	2
AGSR0186	6	8	AR007802	0.033	0.003	25	140	3510	500	3
AGSR0186	8	10	AR007803	0.066	0.01	21	190	8490	300	3
AGSR0186	10	12	AR007804	0.052	0.006	23	110	11800	300	2
AGSR0186	12	14	AR007805	0.084	0.005	25	100	13800	300	4
AGSR0186	14	16	AR007807	0.165	0.008	34	120	12600	200	7
AGSR0186	16	18	AR007808	0.221	0.009	32	130	16700	300	5
AGSR0186	18	20	AR007809	0.267	0.007	44	130	18600	400	6
AGSR0186	20	22	AR007810	0.446	0.014	70	340	19300	300	9
AGSR0186	22	24	AR007811	0.626	0.019	75	470	19900	300	7

Hole	From (m)	To (m)	Sample number	Ni (%)	Co (%)	Sc (g/t)	Mn (ppm)	Cr (ppm)	V (ppm)	Au (ppb)
AGSR0186	24	26	AR007812	0.749	0.023	69	530	17600	200	3
AGSR0186	26	28	AR007813	0.76	0.025	48	610	12000	100	4
AGSR0186	28	30	AR007814	0.774	0.032	43	670	11100	100	4
AGSR0186	30	32	AR007815	0.957	0.041	44	750	11700	100	3
AGSR0186	32	34	AR007817	0.818	0.033	40	970	9920	100	1
AGSR0186	34	36	AR007818	0.817	0.029	43	1010	9430	200	3
AGSR0186	36	38	AR007819	0.837	0.03	42	1180	9790	200	2
AGSR0186	38	40	AR007820	1	0.024	38	980	16700	100	bd
AGSR0186	40	42	AR007821	0.895	0.023	35	1050	16800	100	2
AGSR0186	42	44	AR007822	0.869	0.023	36	1140	15600	100	2
AGSR0186	44	46	AR007823	0.887	0.032	34	1310	14800	100	3
AGSR0186	46	48	AR007824	0.843	0.034	33	1340	14900	100	bd
AGSR0186	48	50	AR007825	0.771	0.035	33	1410	15500	200	4
AGSR0186	50	52	AR007827	0.583	0.028	33	1170	13800	200	4
AGSR0186	52	54	AR007828	0.457	0.028	21	1350	8420	100	5
AGSR0186	54	56	AR007829	0.423	0.033	36	1030	4290	100	1
AGSR0186	56	58	AR007830	1.19	0.077	27	1460	16100	100	119
AGSR0186	58	60	AR007831	1.26	0.068	29	1280	30400	100	395
AGSR0186	60	62	AR007832	1.35	0.067	33	1210	31200	100	113
AGSR0186	62	64	AR007833	0.831	0.049	25	1040	21800	100	44
AGSR0186	64	66	AR007834	1.02	0.064	25	960	22300	100	35
AGSR0186	66	68	AR007835	1.4	0.082	30	1270	29600	100	26
AGSR0186	68	70	AR007837	1.32	0.077	24	1110	26100	100	40
AGSR0186	70	72	AR007838	1.36	0.064	21	930	22000	100	69
AGSR0186	72	74	AR007839	0.862	0.047	12	1000	12800	bd	21
AGSR0186	74	76	AR007840	1.12	0.053	15	740	16800	bd	20
AGSR0186	76	78	AR007841	1.24	0.056	17	780	19200	100	242
AGSR0186	78	80	AR007842	1.11	0.052	16	770	19600	100	21
AGSR0186	80	82	AR007843	0.675	0.036	13	540	12000	bd	60
AGSR0186	82	84	AR007844	0.551	0.03	11	880	8220	bd	75
AGSR0186	84	86	AR007845	0.228	0.014	4	1410	3080	bd	23
AGSR0186	86	88	AR007847	0.142	0.008	4	820	2530	bd	4
AGSR0186	88	90	AR007848	0.259	0.017	4	1050	3260	bd	30
AGSR0186	90	92	AR007849	0.429	0.018	5	440	3320	bd	24
AGSR0186	92	94	AR007850	0.361	0.019	4	1230	3700	bd	15
AGSR0186	94	95	AR007851	0.252	0.015	3	1290	3820	bd	12
AGSR0187	0	2	AR007852	0.027	0.006	16	290	445	100	13
AGSR0187	2	4	AR007853	0.029	0.004	19	160	1120	200	3
AGSR0187	4	6	AR007854	0.02	0.002	18	130	1580	300	bd
AGSR0187	6	8	AR007855	0.025	0.002	27	170	6110	600	2
AGSR0187	8	10	AR007857	0.075	0.011	30	170	2220	300	5
AGSR0187	10	12	AR007858	0.125	0.034	37	460	2220	300	4
AGSR0187	12	14	AR007859	0.13	0.053	37	570	3190	200	2
AGSR0187	14	16	AR007860	0.084	0.009	44	280	7320	300	1
AGSR0187	16	18	AR007861	0.14	0.006	55	180	10800	300	3
AGSR0187	18	20	AR007862	0.165	0.007	68	140	12300	200	5
AGSR0187	20	22	AR007863	0.278	0.008	81	160	16300	300	4
AGSR0187	22	24	AR007864	0.395	0.011	113	290	13000	300	1
AGSR0187	24	26	AR007865	0.514	0.015	125	460	12100	200	5
AGSR0187	26	28	AR007867	0.62	0.026	81	770	12200	200	2
AGSR0187	28	30	AR007868	0.585	0.042	75	900	13000	200	3
AGSR0187	30	32	AR007869	0.551	0.034	68	810	13000	200	2
AGSR0187	32	34	AR007870	0.679	0.032	71	780	14800	200	1
AGSR0187	34	36	AR007871	0.979	0.025	70	880	16700	200	bd
AGSR0187	36	38	AR007872	1.06	0.021	66	910	18700	200	1
AGSR0187	38	40	AR007873	1.37	0.03	56	980	17600	200	1
AGSR0187	40	42	AR007874	1.51	0.03	53	1070	15800	200	bd
AGSR0187	42	44	AR007875	1.31	0.029	43	1200	16200	200	bd
AGSR0187	44	46	AR007877	1.25	0.033	40	1140	17700	100	bd
AGSR0187	46	48	AR007878	1.29	0.033	40	1280	19800	100	bd
AGSR0187	48	50	AR007879	1.45	0.034	36	1340	21300	100	bd
AGSR0187	50	52	AR007880	1.05	0.026	44	1000	16600	200	2
AGSR0187	52	54	AR007881	0.774	0.029	33	1240	12500	100	4
AGSR0187	54	56	AR007882	1.39	0.051	38	1940	15900	100	1
AGSR0187	56	58	AR007883	1.35	0.069	36	2310	13400	100	1
AGSR0187	58	60	AR007884	1.3	0.077	32	2300	11200	100	1
AGSR0187	60	62	AR007885	1.17	0.08	26	2420	11100	100	1
AGSR0187	62	64	AR007887	1.23	0.094	25	3250	9880	100	bd
AGSR0187	64	66	AR007888	1.2	0.103	29	3640	12500	100	1
AGSR0187	66	68	AR007889	1.23	0.237	40	8320	12900	100	bd
AGSR0187	68	70	AR007890	1.2	0.202	35	10300	15700	100	bd
AGSR0187	70	72	AR007891	1.34	0.221	39	13500	18300	100	bd
AGSR0187	72	74	AR007892	1.61	0.253	39	17000	19500	100	bd
AGSR0187	74	76	AR007893	1.5	0.189	36	12100	20300	100	172
AGSR0187	76	78	AR007894	1.43	0.089	39	4830	25400	100	710
AGSR0187	78	80	AR007895	1.41	0.074	39	2590	27800	100	256
AGSR0187	80	82	AR007897	1.24	0.101	33	3990	24100	100	142
AGSR0187	82	84	AR007898	0.664	0.081	14	6460	9610	bd	131
AGSR0187	84	86	AR007899	0.374	0.035	6	5330	3310	bd	34
AGSR0187	86	88	AR007900	0.304	0.026	5	4510	2000	bd	16
AGSR0187	88	90	AR007901	0.348	0.036	4	5470	1750	bd	6
AGSR0187	90	92	AR007902	0.277	0.016	5	1120	1960	bd	9
AGSR0187	92	94	AR007903	0.228	0.01	4	1060	1840	bd	4
AGSR0187	94	95	AR007904	0.241	0.01	5	880	2240	bd	14
AGSR0190	0	2	AR008017	0.011	0.001	10	220	370	100	14
AGSR0190	2	4	AR008019	0.016	0.001	14	170	655	100	3
AGSR0190	4	6	AR008021	0.014	0.001	15	120	1140	200	bd
AGSR0190	6	8	AR008023	0.04	0.003	29	200	2000	200	1
AGSR0190	8	10	AR008025	0.069	0.007	27	250	2320	200	7
AGSR0190	10	12	AR008027	0.06	0.006	24	260	2380	200	11
AGSR0190	12	14	AR008029	0.06	0.008	25	480	1860	200	7
AGSR0190	14	16	AR008031	0.051	0.003	29	290	7390	400	24
AGSR0190	16	18	AR008033	0.108	0.003	43	280	12300	400	4
AGSR0190	18	20	AR008037	0.113	0.002	49	260	16200	500	1
AGSR0190	20	22	AR008039	0.147	0.002	63	120	17200	400	4
AGSR0190	22	24	AR008041	0.171	0.004	68	160	12900	400	3
AGSR0190	24	26	AR008043	0.176	0.003	65	330	13300	500	2
AGSR0190	26	28	AR008045	0.17	0.004	58	350	14800	500	4
AGSR0190	28	30	AR008047	0.193	0.004	65	350	16900	500	2
AGSR0190	30	32	AR008049	0.313	0.004	81	220	22900	500	2
AGSR0190	32	34	AR008051	0.375	0.006	93	260	19300	300	3
AGSR0190	34	36	AR008053	0.447	0.006	104	320	17900	300	7
AGSR0190	36	38	AR008057	0.661	0.008	123	580	20400	300	13
AGSR0190	38	40	AR008059	0.714	0.008	117	600	21700	300	14
AGSR0190	40	42	AR008061	0.776	0.008	120	680	25600	300	1
AGSR0190	42	44	AR008063	0.934	0.018	117	760	26700	300	2
AGSR0190	44	46	AR008065	0.98	0.022	104	780	25700	300	1
AGSR0190	46	48	AR008067	0.994	0.025	95	820	29200	300	bd
AGSR0190	48	50	AR008069	0.952	0.03	84	1000	29700	300	bd
AGSR0190	50	52	AR008071	0.94	0.03	89	1040	32000	300	bd
AGSR0190	52	54	AR008073	0.936	0.027	94	1110	28600	300	1
AGSR0190	54	56	AR008077	0.883	0.026	92	1280	26500	200	bd
AGSR0190	56	58	AR008079	0.768	0.026	84	1340	28500	200	1
AGSR0190	58	60	AR008081	0.745	0.031	72	1750	26600	200	2
AGSR0190	60	62	AR008083	0.488	0.03	37	2290	14800	100	bd
AGSR0190	62	64	AR008085	0.463	0.039	26	1220	9310	100	1
AGSR0190	64	66	AR008087	0.487	0.038	20	4860	6690	bd	bd
AGSR0190	66	68	AR008089	0.404	0.025	12	4250	4390	bd	1
AGSR0190	68	70	AR008091	0.43	0.057	15	8240	5870	bd	1
AGSR0190	70	72	AR008093	0.512	0.093	14	27300	6120	bd	bd
AGSR0190	72	74	AR008097	0.437	0.176	11	63600	4470	bd	5
AGSR0190	74	76	AR008099	0.667	0.361	16	82400	5820	bd	bd
AGSR0190	76	78	AR008101	0.892	0.332	24	51500	8900	100	bd
AGSR0190	78	80	AR008103	1.07	0.182	37	12900	11700	100	5
AGSR0190	80	82	AR008105	1.1	0.158	37	8730	14800	100	4
AGSR0190	82	84	AR008107	1.04	0.109	29	5510	11700	100	4
AGSR0190	84	86	AR008109	1.2	0.077	24	2490	7190	100	140
AGSR0190	86	88	AR008111	1.41	0.075	29	1750	12900	100	51
AGSR0190	88	90	AR008113	1.28	0.07	29	1470	16200	100	83
AGSR0190	90	92	AR008117	1.19	0.082	31	2040	20700	100	95
AGSR0190	92	94	AR008119	1.26	0.104	32	4310	21900	100	64
AGSR0190	94	96	AR008121	1.22	0.102	33	3640	25200	100	53
AGSR0190	96	98	AR008123	1.27	0.092	30	2180	21500	200	50
AGSR0190	98	100	AR008125	1.29	0.098	29	2360	16600	100	42
AGSR0190	100	102	AR008127	1.41	0.103	27	2000	18400	100	41
AGSR0190	102	104	AR008129	1.35	0.111	29	3330	20400	100	65
AGSR0190	104	106	AR008131	1.26	0.087	22	6990	20600	100	81
AGSR0190	106	108	AR008133	1.29	0.072	23	3170	19600	100	43
AGSR0190	108	110	AR008137	0.907	0.043	14	1130	13000	100	40
AGSR0190	110	112	AR008139	0.933	0.041	12	1130	10300	bd	46
AGSR0190	112	114	AR008141	0.945	0.03	11	740	9740	bd	22
AGSR0190	114	116	AR008143	0.872	0.026	10	770	8750	bd	20
AGSR0190	116	118	AR008145	1.23	0.03	12	630	10400	bd	19
AGSR0190	118	120	AR008147	1.11	0.03	11	580	9820	bd	19
AGSR0190	120	122	AR008149	0.817	0.025	8	770	9310	bd	86
AGSR0190	122	124	AR008151	0.652	0.021	8	440	5070	bd	96
AGSR0190	124	126	AR008153	0.709	0.029	7	2180	5040	bd	63
AGSR0190	126	127	AR008155	0.657	0.035	6	3700	3930	bd	16
AGSR0191	0	2	AR008159	0.026	0.002	18	360	605	100	21
AGSR0191	2	4	AR008160	0.035	0.004	21	240	990	200	6
AGSR0191	4	6	AR008162	0.024	0.002	18	160	1360	200	bd
AGSR0191	6	8	AR008163	0.024	0.002	27	130	2290	500	3
AGSR0191	8	10	AR008164	0.112	0.013	45	180	3050	300	4
AGSR0191	10	12	AR008165	0.102	0.013	32	300	2690	200	7
AGSR0191	12	14	AR008166	0.109	0.013	33	210	2290	300	8
AGSR0191	14	16	AR008167	0.108	0.014	34	260	4220	500	4
AGSR0191	16	18	AR008168	0.11	0.01	40	120	4370	500	13
AGSR0191	18	20	AR008169	0.1	0.009	48	120	3570	400	5
AGSR0191	20	22	AR008170	0.11	0.03	71	1360	2050	300	7
AGSR0191	22	24	AR008172	0.15	0.018	92	410	6910	300	1
AGSR0191	24	26	AR008173	0.153	0.028	109	540	6250	400	bd
AGSR0191	26	28	AR008174	0.138	0.038	76	390	6850	400	1
AGSR0191	28	30	AR008175	0.173	0.051	55	1600	5190	300	1
AGSR0191	30	32	AR008176	0.156	0.022	29	1650	6560	200	1
AGSR0191	32	34	AR008177	0.228	0.028	29	2420	6370	200	2
AGSR0191	34	36	AR008178	0.322	0.01	26	490	7760	200	2
AGSR0191	36	38	AR008179	0.279	0.012	20	1700	4910	200	bd
AGSR0191	38	40	AR008180	0.183	0.01	22	460	4710	100	8
AGSR0191	40	42	AR008182	0.1	0.006	41	630	3390	100	6
AGSR0193	0	2	AR008210	0.021	0.002	16	170	525	bd	8
AGSR0193	2	4	AR008212	0.032	0.004	21	190	945	bd	4
AGSR0193	4	6	AR008213	0.032	0.004	21	140	3490	200	5
AGSR0193	6	8	AR008214	0.132	0.009	30	270	15400	100	bd
AGSR0193	8	10	AR008215	0.108	0.007	32	180	17000	bd	bd
AGSR0193	10	12	AR008216	0.195	0.016	27	350	17200	bd	bd
AGSR0193	12	14	AR008217	0.165	0.023	38	410	17600	bd	bd
AGSR0193	14	16	AR008218	0.171	0.021	34	480	19600	bd	bd
AGSR0193	16	18	AR008219	0.336	0.023	54	390	30900	100	3
AGSR0193	18	20	AR008220	0.31	0.018	40	310	17100	bd	4
AGSR0193	20	22	AR008222	0.351	0.017	30	380	11500	bd	7
AGSR0193	22	24	AR008223	0.534	0.025	31	540	11400	bd	10
AGSR0193	24	26	AR008224	0.492	0.021	22	620	8650	bd	4
AGSR0193	26	28	AR008225	0.398	0.018	13	560	6810	bd	10
AGSR0193	28	30	AR008226	0.358	0.023	11	1230	6230	bd	6
AGSR0193	30	32	AR008227	0.432	0.041	8	2200	5990	bd	4
AGSR0193	32	34	AR008228	0.521	0.047	12	2300	7340	bd	4

Hole	From (m)	To (m)	Sample number	Ni (%)	Co (%)	Sc (g/t)	Mn (ppm)	Cr (ppm)	V (ppm)	Au (ppb)
AGSR0193	34	36	AR008229	0.617	0.056	12	3240	7010	bd	5
AGSR0193	36	38	AR008230	0.521	0.077	8	10400	5970	bd	3
AGSR0193	38	40	AR008232	0.492	0.042	8	4410	5140	bd	3
AGSR0193	40	42	AR008233	0.382	0.024	5	2350	3750	bd	1
AGSR0193	42	44	AR008234	0.293	0.014	3	1160	4130	bd	1
AGSR0193	44	46	AR008235	0.291	0.012	3	920	3970	bd	1
AGSR0193	46	48	AR008236	0.374	0.019	4	1860	3370	bd	1
AGSR0194	0	2	AR008237	0.018	0.002	7	250	465	bd	5
AGSR0194	2	4	AR008238	0.052	0.002	22	330	2830	200	5
AGSR0194	4	6	AR008239	0.065	0.006	23	430	7880	200	2
AGSR0194	6	8	AR008240	0.175	0.009	24	330	15400	100	bd
AGSR0194	8	10	AR008242	0.105	0.004	24	170	18500	bd	bd
AGSR0194	10	12	AR008243	0.149	0.016	27	220	10800	bd	bd
AGSR0194	12	14	AR008244	0.154	0.029	39	420	10400	bd	bd
AGSR0194	14	16	AR008245	0.167	0.018	31	330	10100	bd	bd
AGSR0194	16	18	AR008246	0.235	0.013	38	200	10800	bd	1
AGSR0194	18	20	AR008247	0.352	0.018	40	370	11800	bd	2
AGSR0194	20	22	AR008248	0.321	0.014	21	420	8240	bd	9
AGSR0194	22	24	AR008249	0.556	0.022	19	510	7020	bd	8
AGSR0194	24	26	AR008250	0.654	0.026	18	650	7080	bd	7
AGSR0194	26	28	AR008252	0.618	0.025	16	700	6560	bd	12
AGSR0194	28	30	AR008253	0.644	0.024	16	660	7380	bd	8
AGSR0194	30	32	AR008254	0.597	0.025	17	810	8850	bd	5
AGSR0194	32	34	AR008255	0.429	0.018	9	1240	6040	bd	5
AGSR0194	34	36	AR008256	0.487	0.022	7	1490	8060	bd	2
AGSR0194	36	38	AR008257	0.38	0.017	5	1370	7840	bd	1
AGSR0194	38	40	AR008258	0.371	0.018	5	1360	7220	bd	1
AGSR0194	40	41	AR008259	0.273	0.01	4	930	4690	bd	2
AGSR0291	0	2	AR010945	0.017	0.002	15	300	490	100	6
AGSR0291	2	4	AR010946	0.021	0.003	19	200	685	100	4
AGSR0291	4	6	AR010947	0.018	bd	21	110	1860	300	4
AGSR0291	6	8	AR010948	0.021	0.001	25	70	2340	400	3
AGSR0291	8	10	AR010950	0.072	0.008	45	90	3100	300	13
AGSR0291	10	12	AR010951	0.153	0.02	43	350	4260	300	7
AGSR0291	12	14	AR010952	0.135	0.018	39	290	3430	300	6
AGSR0291	14	16	AR010953	0.106	0.018	38	290	2620	200	6
AGSR0291	16	18	AR010954	0.087	0.013	37	220	2390	200	14
AGSR0291	18	20	AR010955	0.069	0.006	33	90	1790	100	6
AGSR0291	20	22	AR010956	0.065	0.006	30	140	1370	100	5
AGSR0291	22	24	AR010957	0.063	0.005	29	170	3150	400	3
AGSR0291	24	26	AR010958	0.1	0.01	36	290	3070	400	3
AGSR0291	26	28	AR010960	0.044	0.003	37	340	2400	100	2
AGSR0291	28	30	AR010961	0.072	0.005	56	290	4360	200	2
AGSR0291	30	31	AR010962	0.113	0.031	86	2260	4430	400	2
AGSR0292	0	2	AR010963	0.015	0.001	12	200	560	100	10
AGSR0292	2	4	AR010964	0.014	0.001	17	140	635	100	3
AGSR0292	4	6	AR010965	0.021	0.001	23	140	1200	200	5
AGSR0292	6	8	AR010966	0.033	0.003	28	170	1560	200	3
AGSR0292	8	10	AR010967	0.063	0.006	49	240	3610	700	4
AGSR0292	10	12	AR010968	0.122	0.026	57	400	3440	300	61
AGSR0292	12	14	AR010970	0.127	0.02	52	230	3870	300	157
AGSR0292	14	16	AR010971	0.104	0.014	43	220	2790	300	13
AGSR0292	16	18	AR010972	0.073	0.012	36	270	2020	200	9
AGSR0292	18	20	AR010973	0.061	0.007	35	190	1670	100	5
AGSR0292	20	22	AR010974	0.064	0.008	40	280	1500	100	4
AGSR0292	22	24	AR010975	0.055	0.006	30	270	3180	300	4
AGSR0292	24	26	AR010976	0.05	0.004	36	150	5050	600	2
AGSR0292	26	28	AR010977	0.067	0.004	68	150	5030	400	3
AGSR0292	28	30	AR010978	0.048	0.003	62	210	4080	300	3
AGSR0293	0	2	AR010980	0.02	0.002	17	210	880	100	8
AGSR0293	2	4	AR010981	0.016	bd	24	110	2060	400	1
AGSR0293	4	6	AR010982	0.017	0.002	19	230	805	100	7
AGSR0293	6	8	AR010983	0.011	bd	23	70	2610	600	2
AGSR0293	8	10	AR010984	0.065	0.005	36	120	3900	600	3
AGSR0293	10	12	AR010985	0.142	0.019	41	330	3460	300	7
AGSR0293	12	14	AR010986	0.134	0.014	42	170	3730	300	8
AGSR0293	14	16	AR010987	0.095	0.012	34	180	2900	300	5
AGSR0293	16	18	AR010988	0.035	0.003	10	180	985	bd	2
AGSR0293	18	20	AR010990	0.034	0.005	9	390	970	bd	3
AGSR0293	20	22	AR010991	0.082	0.01	39	190	2140	200	6
AGSR0293	22	24	AR010992	0.07	0.005	30	140	2230	200	4
AGSR0293	24	26	AR010993	0.087	0.007	31	90	2320	200	3
AGSR0293	26	28	AR010994	0.083	0.006	31	80	2300	100	4
AGSR0293	28	30	AR010995	0.069	0.004	31	90	2380	100	4
AGSR0293	30	32	AR010996	0.059	0.004	30	120	2010	100	4
AGSR0293	32	34	AR010997	0.039	0.006	53	390	2870	300	2
AGSR0293	34	35	AR010998	0.045	0.008	56	460	3430	300	5
AGSR0294	0	2	AR011000	0.017	0.004	14	220	620	100	5
AGSR0294	2	4	AR011002	0.015	0.001	22	150	1210	200	3
AGSR0294	4	6	AR011003	0.027	0.004	37	430	2540	600	2
AGSR0294	6	8	AR011004	0.07	0.01	38	1260	2250	400	2
AGSR0294	8	10	AR011005	0.156	0.026	21	1530	1990	100	3
AGSR0294	10	12	AR011006	0.292	0.02	16	250	2770	100	5
AGSR0294	12	14	AR011007	0.22	0.004	8	80	1930	bd	3
AGSR0294	14	16	AR011008	0.064	0.001	6	20	990	bd	2
AGSR0294	16	18	AR011009	0.4	0.032	27	1630	16100	200	6
AGSR0294	18	20	AR011010	0.889	0.09	40	6730	21600	100	1
AGSR0294	20	22	AR011012	1	0.162	43	7470	17900	100	4
AGSR0294	22	24	AR011013	1.01	0.146	47	7040	18600	100	2
AGSR0294	24	26	AR011014	1.01	0.083	44	3480	17000	100	2
AGSR0294	26	28	AR011015	1.25	0.056	33	2210	28100	100	2
AGSR0294	28	30	AR011016	1.46	0.038	36	2010	14500	100	1
AGSR0294	30	32	AR011017	1	0.033	25	1190	13500	100	3

Hole	From (m)	To (m)	Sample number	Ni (%)	Co (%)	Sc (g/t)	Mn (ppm)	Cr (ppm)	V (ppm)	Au (ppb)
AGSR0294	32	34	AR011018	0.441	0.031	17	1330	5750	100	3
AGSR0294	34	36	AR011019	0.743	0.041	23	1750	7970	100	2
AGSR0294	36	38	AR011020	0.358	0.015	8	790	7090	bd	5
AGSR0294	38	40	AR011022	0.205	0.009	5	460	5730	bd	5
AGSR0294	40	42	AR011023	0.212	0.011	6	450	6700	bd	4
AGSR0294	42	44	AR011024	0.418	0.021	9	2210	16700	bd	5
AGSR0294	44	46	AR011025	0.284	0.013	6	1790	13700	bd	12
AGSR0294	46	48	AR011026	0.504	0.026	6	2260	11400	bd	4
AGSR0294	48	50	AR011027	0.367	0.017	5	2040	10000	bd	4
AGSR0294	50	51	AR011028	0.362	0.027	4	1550	5670	bd	6
AGSR0295	0	2	AR011029	0.018	0.001	9	150	455	100	6
AGSR0295	2	4	AR011030	0.01	0.001	9	120	390	100	5
AGSR0295	4	6	AR011032	0.033	0.003	37	520	2680	500	2
AGSR0295	6	8	AR011033	0.024	0.001	28	280	1970	400	3
AGSR0295	8	10	AR011034	0.069	0.01	9	3310	560	bd	4
AGSR0295	10	12	AR011035	0.097	0.018	6	1460	685	bd	4
AGSR0295	12	14	AR011036	0.049	0.004	7	100	635	bd	2
AGSR0295	14	16	AR011037	0.041	0.002	6	40	310	bd	1
AGSR0295	16	18	AR011038	0.139	0.006	11	230	6460	200	1
AGSR0295	18	20	AR011039	0.382	0.03	20	1290	16600	300	1
AGSR0295	20	22	AR011040	0.817	0.106	34	8510	16400	200	1
AGSR0295	22	24	AR011042	0.567	0.071	44	1940	10000	100	1
AGSR0295	24	26	AR011043	0.374	0.041	25	1420	3850	bd	1
AGSR0295	26	28	AR011044	0.218	0.014	24	590	3150	100	1
AGSR0295	28	30	AR011045	0.505	0.024	29	630	5800	bd	1
AGSR0295	30	32	AR011046	0.317	0.029	13	1000	1370	bd	2
AGSR0295	32	34	AR011047	0.271	0.03	12	1080	675	bd	2
AGSR0295	34	36	AR011048	0.301	0.026	16	950	2090	100	5
AGSR0295	36	38	AR011049	0.277	0.016	14	610	1750	100	2
AGSR0295	38	40	AR011050	0.301	0.013	13	400	845	100	3
AGSR0295	40	42	AR011052	0.266	0.014	15	490	1550	100	4
AGSR0295	42	44	AR011053	0.383	0.008	11	240	690	bd	3
AGSR0295	44	46	AR011054	0.401	0.01	11	280	455	bd	3
AGSR0295	46	48	AR011055	0.4	0.008	11	280	465	bd	2
AGSR0295	48	50	AR011056	0.473	0.009	10	300	340	bd	bd
AGSR0295	50	52	AR011057	0.639	0.015	9	290	280	bd	4
AGSR0295	52	53	AR011058	0.687	0.016	9	280	275	bd	78
AGSR0373	0	2	AR013660	0.048	0.002	8	230	1470	100	12
AGSR0373	2	4	AR013661	0.029	0.002	12	180	895	100	3
AGSR0373	4	6	AR013663	0.039	0.001	23	190	2430	200	3
AGSR0373	6	8	AR013664	0.124	bd	25	220	7030	100	2
AGSR0373	8	10	AR013665	0.283	0.005	33	380	19700	200	1
AGSR0373	10	12	AR013666	0.288	0.017	25	650	22400	200	10
AGSR0373	12	14	AR013667	0.334	0.013	22	460	19800	bd	2
AGSR0373	14	16	AR013668	0.357	0.013	25	550	10400	bd	1
AGSR0373	16	18	AR013669	0.25	0.011	21	340	14200	bd	3
AGSR0373	18	20	AR013670	0.159	0.007	9	240	3920	bd	9
AGSR0373	20	22	AR013671	0.183	0.009	16	260	6920	bd	7
AGSR0373	22	24	AR013673	0.184	0.009	17	270	8120	bd	10
AGSR0373	24	26	AR013674	0.493	0.022	25	340	6570	bd	7
AGSR0373	26	28	AR013675	0.635	0.031	20	600	5230	bd	6
AGSR0373	28	30	AR013676	0.783	0.119	21	4070	5650	bd	8
AGSR0374	0	2	AR013677	0.102	0.013	9	740	875	100	11
AGSR0374	2	4	AR013678	0.03	0.002	10	170	575	100	2
AGSR0374	4	6	AR013679	0.031	0.001	19	180	1810	200	3
AGSR0374	6	8	AR013680	0.037	bd	23	200	2230	200	1
AGSR0374	8	10	AR013681	0.118	0.019	13	460	6580	bd	2
AGSR0374	10	12	AR013683	0.129	0.013	12	340	5190	bd	3
AGSR0374	12	14	AR013684	0.152	0.007	8	150	2410	bd	1
AGSR0374	14	16	AR013685	0.085	0.003	7	110	2980	bd	3
AGSR0374	16	18	AR013686	0.391	0.015	24	260	5380	bd	1
AGSR0374	18	20	AR013687	0.53	0.019	27	280	7040	bd	8
AGSR0374	20	22	AR013688	0.429	0.021	33	230	9400	bd	3
AGSR0374	22	24	AR013689	0.551	0.024	29	330	5750	bd	5
AGSR0374	24	26	AR013690	0.491	0.02	24	310	4610	bd	7
AGSR0374	26	28	AR013691	0.386	0.019	17	520	3300	bd	9
AGSR0375	0	2	AR013693	0.037	0.003	10	450	510	bd	8
AGSR0375	2	4	AR013694	0.033	0.005	12	360	515	100	7
AGSR0375	4	6	AR013695	0.091	0.024	43	590	3420	700	7
AGSR0375	6	8	AR013696	0.242	0.02	23	520	7450	200	bd
AGSR0375	8	10	AR013697	0.403	0.018	29	530	9620	bd	1
AGSR0375	10	12	AR013698	0.386	0.018	29	400	9590	100	bd
AGSR0375	12	14	AR013699	0.181	0.013	51	330	6630	100	1
AGSR0375	14	16	AR013700	0.305	0.025	30	630	6170	bd	2
AGSR0375	16	18	AR013701	0.484	0.035	43	580	8440	bd	1
AGSR0375	18	20	AR013703	0.433	0.03	51	360	8560	bd	3
AGSR0375	20	22	AR013704	0.613	0.044	52	580	9230	bd	1
AGSR0375	22	24	AR013705	0.685	0.055	39	530	6940	bd	4
AGSR0375	24	26	AR013706	0.873	0.044	42	470	10300	100	1
AGSR0375	26	28	AR013707	0.552	0.026	28	410	7530	bd	4
AGSR0377	0	2	AR013727	0.312	0.026	11	720	1460	bd	13
AGSR0377	2	4	AR013728	0.153	0.014	17	410	975	100	7
AGSR0377	4	6	AR013729	0.299	0.025	14	830	1840	100	7
AGSR0377	6	8	AR013730	0.141	0.008	23	310	9020	200	1
AGSR0377	8	10	AR013731	0.235	0.012	32	310	9830	100	2
AGSR0377	10	12	AR013733	0.202	0.015	27	740	8140	100	2
AGSR0377	12	14	AR013734	0.235	0.017	23	590	8050	100	1
AGSR0377	14	16	AR013735	0.307	0.021	27	410	8310	100	1
AGSR0377	16	18	AR013736	0.276	0.014	30	200	8460	100	1
AGSR0377	18	20	AR013737	0.371	0.017	34	170	8500	bd	2
AGSR0377	20	22	AR013738	0.469	0.023	32	410	7700	bd	5
AGSR0377	22	24	AR013739	0.606	0.027	27	470	5040	bd	4
AGSR0377	24	26	AR013740	0.53	0.022	19	380	3850	bd	9

Hole	From (m)	To (m)	Sample number	Ni (%)	Co (%)	Sc (g/t)	Mn (ppm)	Cr (ppm)	V (ppm)	Au (ppb)
AGSR0377	26	28	AR013741	0.39	0.017	15	340	2930	bd	3
AGSR0377	28	30	AR013743	0.607	0.041	10	830	1930	bd	7
AGSR0377	30	31	AR013744	0.939	0.079	9	1660	1940	bd	1
AGSR0380	0	2	AR013775	0.053	0.005	9	310	400	bd	6
AGSR0380	2	4	AR013776	0.048	0.007	14	230	655	100	4
AGSR0380	4	6	AR013777	0.045	0.002	29	200	2210	400	2
AGSR0380	6	8	AR013778	0.035	0.003	21	120	1250	200	bd
AGSR0380	8	10	AR013779	0.113	0.009	17	200	8170	200	1
AGSR0380	10	12	AR013780	0.22	0.01	27	350	14100	100	2
AGSR0380	12	14	AR013781	0.104	0.006	26	170	14400	200	3
AGSR0380	14	16	AR013783	0.145	0.012	41	80	13500	200	3
AGSR0380	16	18	AR013784	0.296	0.026	38	220	11500	100	1
AGSR0380	18	20	AR013785	0.579	0.048	34	480	12600	100	1
AGSR0380	20	22	AR013786	0.842	0.041	31	620	22500	100	6
AGSR0380	22	24	AR013787	1.14	0.058	25	1180	22700	100	bd
AGSR0380	24	25	AR013788	1.32	0.065	29	1440	23000	100	2
AGSR0411	0	2	AR019201	0.03	0.002	11	300	525	bd	10
AGSR0411	2	4	AR019202	0.034	0.002	18	160	835	100	3
AGSR0411	4	6	AR019203	0.036	bd	26	210	3980	300	1
AGSR0411	6	8	AR019204	0.026	0.001	18	220	4000	400	2
AGSR0411	8	10	AR019205	0.027	0.001	20	170	4380	400	2
AGSR0411	10	12	AR019206	0.086	0.002	37	200	9210	300	bd
AGSR0411	12	14	AR019208	0.106	0.002	46	130	9020	100	bd
AGSR0411	14	16	AR019209	0.213	0.005	56	250	15200	200	bd
AGSR0411	16	18	AR019210	0.271	0.005	49	270	16000	200	bd
AGSR0411	18	20	AR019211	0.435	0.045	25	940	13600	100	1
AGSR0411	20	22	AR019212	0.409	0.04	23	710	6900	100	3
AGSR0411	22	24	AR019213	0.597	0.032	14	590	5980	bd	bd
AGSR0411	24	26	AR019214	0.674	0.035	20	600	7450	bd	3
AGSR0411	26	28	AR019215	0.775	0.049	17	710	7630	bd	5
AGSR0411	28	30	AR019216	0.636	0.025	15	390	6970	bd	3
AGSR0411	30	32	AR019218	0.769	0.058	14	950	4200	bd	2
AGSR0411	32	34	AR019219	0.725	0.049	17	880	4770	bd	2
AGSR0411	34	36	AR019220	0.754	0.048	16	820	5740	bd	4
AGSR0411	36	38	AR019221	0.73	0.046	20	900	6120	bd	2
AGSR0411	38	40	AR019222	1.28	0.086	22	1890	4630	bd	3
AGSR0411	40	42	AR019223	1.26	0.079	18	1700	3930	bd	4
AGSR0411	42	44	AR019224	1.27	0.072	17	1850	3980	bd	4
AGSR0411	44	46	AR019225	1.1	0.064	18	2060	4750	bd	5
AGSR0411	46	48	AR019226	0.919	0.044	16	1490	5060	bd	3
AGSR0411	48	50	AR019228	0.696	0.039	10	1910	2830	bd	2
AGSR0411	50	52	AR019229	0.688	0.014	5	1070	1580	bd	2
AGSR0411	52	54	AR019230	0.652	0.02	7	1570	2090	bd	2
AGSR0411	54	56	AR019231	0.352	0.008	4	780	1410	bd	10
AGSR0411	56	58	AR019232	0.324	0.009	4	820	1490	bd	26
AGSR0411	58	60	AR019233	0.308	0.007	4	690	1770	bd	53
AGSR0411	60	62	AR019234	0.228	0.007	4	610	1080	bd	9
AGSR0411	62	64	AR019235	0.23	0.009	5	740	1370	bd	2
AGSR0411	64	66	AR019236	0.265	0.011	4	900	1660	bd	14
AGSR0411	66	68	AR019238	0.345	0.017	7	1320	2550	bd	22
AGSR0411	68	70	AR019239	0.257	0.01	5	890	1980	bd	4
AGSR0411	70	72	AR019240	0.259	0.011	5	890	1760	bd	3
AGSR0411	72	74	AR019241	0.272	0.011	5	1310	3310	bd	5
AGSR0411	74	76	AR019242	0.282	0.013	4	1660	4030	bd	66
AGSR0411	76	78	AR019243	0.55	0.031	7	3140	6360	bd	44
AGSR0411	78	80	AR019244	0.606	0.028	9	1870	7230	bd	7
AGSR0411	80	82	AR019245	0.63	0.028	8	1620	5010	bd	9
AGSR0411	82	84	AR019246	0.544	0.022	9	950	5000	bd	10
AGSR0411	84	86	AR019248	0.706	0.031	8	1410	8780	bd	10
AGSR0411	86	88	AR019249	0.829	0.032	9	1210	9190	bd	10
AGSR0411	88	90	AR019250	0.978	0.032	13	1070	11300	bd	7
AGSR0411	90	92	AR019251	0.949	0.038	14	1080	14000	bd	13
AGSR0411	92	94	AR019252	0.619	0.043	9	6450	7420	bd	19
AGSR0411	94	96	AR019253	0.669	0.049	8	8240	5960	bd	31
AGSR0411	96	98	AR019254	0.463	0.025	5	3010	3880	bd	22
AGSR0411	98	100	AR019255	0.457	0.019	7	2140	4750	bd	20
AGSR0411	100	102	AR019256	0.313	0.013	4	1400	3070	bd	4
AGSR0411	102	104	AR019258	0.36	0.013	5	1450	2830	bd	3
AGSR0411	104	106	AR019259	0.301	0.011	4	1780	2640	bd	2
AGSR0411	106	108	AR019260	0.326	0.013	5	1460	3120	bd	2
AGSR0411	108	110	AR019261	0.266	0.011	4	1310	2380	bd	1
AGSR0412	0	2	AR019262	0.022	0.001	8	210	350	bd	10
AGSR0412	2	4	AR019263	0.027	0.001	21	150	1530	100	3
AGSR0412	4	6	AR019264	0.027	bd	24	150	2540	200	1
AGSR0412	6	8	AR019265	0.029	bd	25	150	2750	200	1
AGSR0412	8	10	AR019266	0.036	0.002	21	150	4370	200	2
AGSR0412	10	12	AR019268	0.243	0.007	36	320	15600	200	bd
AGSR0412	12	14	AR019269	0.333	0.014	37	490	19700	200	bd
AGSR0412	14	16	AR019270	0.339	0.019	39	420	26900	300	bd
AGSR0412	16	18	AR019271	0.197	0.01	35	280	25000	200	2
AGSR0412	18	20	AR019272	0.248	0.012	46	240	22500	200	2
AGSR0412	20	22	AR019273	0.42	0.018	65	340	31300	200	2
AGSR0412	22	24	AR019274	0.562	0.035	87	460	33000	200	3
AGSR0412	24	26	AR019275	0.628	0.03	84	780	58800	200	4
AGSR0412	26	28	AR019276	0.633	0.029	75	660	44300	200	5
AGSR0412	28	30	AR019278	0.713	0.04	67	770	35300	100	4
AGSR0412	30	32	AR019279	0.931	0.107	33	2190	15000	bd	3
AGSR0412	32	34	AR019280	1.11	0.145	30	2370	14800	bd	2
AGSR0412	34	36	AR019281	1.32	0.159	31	2320	16900	bd	3
AGSR0412	36	38	AR019282	1.3	0.12	41	1870	36200	100	3
AGSR0412	38	40	AR019283	1.08	0.069	34	1070	30700	100	2
AGSR0412	40	42	AR019284	1.09	0.064	33	960	31400	100	3
AGSR0412	42	44	AR019285	1.46	0.076	32	860	24400	100	2
AGSR0412	44	46	AR019286	1.07	0.057	23	710	16400	bd	2
AGSR0412	46	48	AR019288	1.22	0.06	30	830	13900	100	2
AGSR0412	48	50	AR019289	1.17	0.059	25	970	12000	bd	1
AGSR0412	50	52	AR019290	0.61	0.036	13	1310	7290	bd	5
AGSR0412	52	54	AR019291	0.388	0.018	7	920	5680	bd	7
AGSR0412	54	56	AR019292	0.571	0.03	13	1020	5800	bd	3
AGSR0412	56	58	AR019293	0.494	0.027	15	1020	4790	bd	4
AGSR0412	58	60	AR019294	0.505	0.026	10	1260	4540	bd	15
AGSR0412	60	62	AR019295	0.212	0.008	4	770	1880	bd	11
AGSR0412	62	64	AR019296	0.221	0.009	4	780	2570	bd	4
AGSR0412	64	66	AR019298	0.215	0.007	4	640	3690	bd	56
AGSR0412	66	68	AR019299	0.489	0.024	4	1710	3530	bd	8
AGSR0412	68	70	AR019300	0.989	0.059	12	3070	7530	bd	7
AGSR0412	70	72	AR019301	0.623	0.044	7	3960	3970	bd	9
AGSR0412	72	74	AR019302	0.394	0.027	4	2810	2610	bd	29
AGSR0412	74	76	AR019303	0.384	0.028	5	2380	4920	bd	51
AGSR0412	76	78	AR019304	0.368	0.021	6	760	3190	bd	305
AGSR0412	78	80	AR019305	0.249	0.01	4	1050	2380	bd	16
AGSR0412	80	82	AR019306	0.213	0.008	6	770	955	bd	15
AGSR0412	82	84	AR019308	0.238	0.01	5	930	935	bd	5
AGSR0412	84	86	AR019309	0.2	0.008	4	940	800	bd	2
AGSR0412	86	88	AR019310	0.28	0.011	6	940	1120	bd	3
AGSR0412	88	90	AR019311	0.222	0.008	4	930	855	bd	1
AGSR0412	90	92	AR019312	0.249	0.009	5	880	1010	bd	2
AGSR0412	92	94	AR019313	0.281	0.01	5	880	1120	bd	3
AGSR0412	94	96	AR019314	0.274	0.011	5	870	1260	bd	2
AGSR0412	96	98	AR019315	0.285	0.011	6	920	1250	bd	2
AGSR0412	98	100	AR019316	0.288	0.011	6	940	1290	bd	1
AGSR0412	100	102	AR019318	0.274	0.01	6	980	1260	bd	1
AGSR0412	102	104	AR019319	0.293	0.012	6	950	1370	bd	bd
AGSR0412	104	106	AR019320	0.285	0.012	6	1040	1310	bd	2
AGSR0412	106	108	AR019321	0.284	0.011	6	860	1320	bd	bd
AGSR0412	108	110	AR019322	0.288	0.011	6	830	1430	bd	2
AGSR0412	110	112	AR019323	0.292	0.012	6	860	1630	bd	1
AGSR0412	112	114	AR019324	0.286	0.012	6	840	1550	bd	3
AGSR0412	114	116	AR019325	0.271	0.011	6	880	1570	bd	1
AGSR0412	116	118	AR019326	0.273	0.011	5	870	2000	bd	2
AGSR0412	118	120	AR019328	0.275	0.011	5	810	1910	bd	2
AGSR0412	120	122	AR019329	0.276	0.011	6	870	1980	bd	2
AGSR0412	122	124	AR019330	0.279	0.012	6	910	1980	bd	1
AGSR0412	124	126	AR019331	0.275	0.012	5	900	3290	bd	1
AGSR0412	126	128	AR019332	0.25	0.011	6	1100	4070	bd	3
AGSR0412	128	130	AR019333	0.226	0.011	8	880	3730	bd	1
AGSR0412	130	132	AR019334	0.199	0.011	8	950	5100	bd	1
AGSR0412	132	134	AR019335	0.186	0.013	8	1020	5740	bd	bd
AGSR0412	134	136	AR019336	0.396	0.028	8	2770	7280	bd	2
AGSR0412	136	138	AR019338	0.557	0.035	7	3260	6880	bd	2
AGSR0412	138	140	AR019339	0.459	0.027	6	3070	4740	bd	3
AGSR0412	140	142	AR019340	1.13	0.108	6	5920	6250	bd	9
AGSR0412	142	144	AR019341	0.833	0.063	7	5230	6780	bd	5
AGSR0412	144	146	AR019342	0.891	0.024	11	1010	11100	bd	6
AGSR0412	146	148	AR019343	0.796	0.024	9	1270	9890	bd	4
AGSR0412	148	150	AR019344	0.805	0.022	9	1040	9170	bd	4
AGSR0413	0	2	AR019345	0.02	0.001	12	220	380	bd	12
AGSR0413	2	4	AR019346	0.034	0.004	16	190	550	100	6
AGSR0413	4	6	AR019348	0.03	0.001	24	160	2600	300	1
AGSR0413	6	8	AR019349	0.029	bd	19	70	3050	300	2
AGSR0413	8	10	AR019350	0.033	0.001	15	50	2770	300	2
AGSR0413	10	12	AR019351	0.035	0.001	17	100	3830	300	1
AGSR0413	12	14	AR019352	0.053	0.003	19	300	8750	400	bd
AGSR0413	14	16	AR019353	0.12	0.004	59	190	11800	300	1
AGSR0413	16	18	AR019354	0.183	0.011	63	240	7920	100	bd
AGSR0413	18	20	AR019355	0.252	0.014	52	310	8690	100	bd
AGSR0413	20	22	AR019356	0.264	0.008	71	240	14800	100	3
AGSR0413	22	24	AR019358	0.431	0.013	57	350	14900	100	3
AGSR0413	24	26	AR019359	0.509	0.018	60	480	9550	bd	4
AGSR0413	26	28	AR019360	0.544	0.017	50	300	14600	bd	1
AGSR0413	28	30	AR019361	0.642	0.016	58	250	19800	100	2
AGSR0413	30	32	AR019362	0.711	0.015	61	320	20900	100	2
AGSR0413	32	34	AR019363	0.686	0.021	43	630	15700	100	2
AGSR0413	34	36	AR019364	0.906	0.025	54	810	23200	100	1
AGSR0413	36	38	AR019365	1.31	0.044	66	1160	31500	100	bd
AGSR0413	38	40	AR019366	1.05	0.038	68	980	25700	200	bd
AGSR0413	40	42	AR019368	0.668	0.032	45	820	16200	100	1
AGSR0413	42	44	AR019369	0.668	0.035	40	950	14700	100	1
AGSR0413	44	46	AR019370	1.11	0.092	37	6200	17900	100	bd
AGSR0413	46	48	AR019371	1.31	0.162	39	11800	21700	100	2
AGSR0413	48	50	AR019372	1.34	0.125	38	7080	22900	100	2
AGSR0413	50	52	AR019373	1.02	0.062	35	2680	22000	100	bd
AGSR0413	52	54	AR019374	0.848	0.084	30	3210	17000	100	bd
AGSR0413	54	56	AR019375	1.04	0.188	36	9120	12900	100	1
AGSR0413	56	58	AR019376	1.21	0.042	38	2980	13200	200	3
AGSR0413	58	60	AR019378	1.21	0.038	34	2390	12400	100	2
AGSR0413	60	62	AR019379	1.31	0.034	34	1640	12800	100	bd
AGSR0413	62	64	AR019380	0.89	0.026	48	1440	15600	100	bd
AGSR0413	64	66	AR019381	1.02	0.029	42	1260	13700	100	bd
AGSR0413	66	68	AR019382	1.14	0.16	37	10300	12500	100	bd
AGSR0413	68	70	AR019383	1.27	0.283	36	21000	8920	100	bd
AGSR0413	70	72	AR019384	1.34	0.196	35	11100	8750	100	bd
AGSR0413	72	74	AR019385	1.54	0.25	35	10700	10500	100	bd
AGSR0413	74	76	AR019386	1.45	0.246	35	11100	9640	100	bd
AGSR0413	76	78	AR019388	1.36	0.216	36	9600	8720	100	bd
AGSR0413	78	80	AR019389	1.41	0.26	33	12300	8040	100	bd

Hole	From (m)	To (m)	Sample number	Ni (%)	Co (%)	Sc (g/t)	Mn (ppm)	Cr (ppm)	V (ppm)	Au (ppb)
AGSR0413	80	82	AR019390	1.41	0.116	35	5150	9250	100	1
AGSR0413	82	84	AR019391	1.52	0.074	34	3090	9770	100	bd
AGSR0413	84	86	AR019392	1.39	0.062	32	2450	9440	100	bd
AGSR0413	86	88	AR019393	1.37	0.062	33	2010	11700	100	1
AGSR0413	88	90	AR019394	1.34	0.162	33	4820	10700	100	11
AGSR0413	90	92	AR019395	1.39	0.094	34	2750	16100	100	bd
AGSR0413	92	94	AR019396	1.32	0.058	24	2860	13700	100	3
AGSR0413	94	96	AR019398	1.09	0.027	14	1910	10600	bd	20
AGSR0413	96	98	AR019399	0.995	0.019	13	1550	8430	bd	19
AGSR0413	98	100	AR019400	0.718	0.019	8	1530	5250	bd	23
AGSR0413	100	102	AR019401	0.343	0.01	5	1040	1860	bd	10
AGSR0413	102	104	AR019402	0.303	0.012	4	1150	1740	bd	11
AGSR0413	104	106	AR019403	0.317	0.014	5	1380	2040	bd	2
AGSR0413	106	108	AR019404	0.52	0.011	6	1030	2580	bd	17
AGSR0413	108	110	AR019405	0.438	0.011	5	920	2430	bd	21
AGSR0413	110	112	AR019406	0.294	0.014	3	1490	1240	bd	10
AGSR0413	112	114	AR019408	0.364	0.021	3	2230	1520	bd	20
AGSR0413	114	116	AR019409	0.564	0.009	7	880	4140	bd	6
AGSR0413	116	118	AR019410	0.728	0.013	12	1120	8990	bd	11
AGSR0413	118	120	AR019411	0.692	0.014	12	970	10300	bd	6
AGSR0414	0	2	AR019412	0.029	0.003	16	340	520	100	11
AGSR0414	2	4	AR019413	0.067	0.025	17	380	595	100	6
AGSR0414	4	6	AR019414	0.042	0.004	20	120	2030	200	3
AGSR0414	6	8	AR019415	0.049	0.011	16	500	7540	300	2
AGSR0414	8	10	AR019416	0.158	0.028	43	700	13600	200	bd
AGSR0414	10	12	AR019418	0.052	0.015	54	360	9850	200	1
AGSR0414	12	14	AR019419	0.037	0.016	49	450	4840	100	1
AGSR0414	14	16	AR019420	0.197	0.247	44	14300	3370	100	1
AGSR0414	16	18	AR019421	0.683	0.84	61	51900	2730	100	1
AGSR0414	18	20	AR019422	0.217	0.029	85	1250	11600	200	1
AGSR0414	20	22	AR019423	0.35	0.033	76	1090	9330	200	bd
AGSR0414	22	24	AR019424	0.637	0.052	78	930	12100	100	3
AGSR0414	24	26	AR019425	0.773	0.053	57	1040	10400	100	3
AGSR0414	26	28	AR019426	0.896	0.047	49	900	11000	100	4
AGSR0414	28	30	AR019428	1.03	0.045	45	890	14000	100	3
AGSR0414	30	32	AR019429	1.05	0.045	43	1110	15400	100	2
AGSR0414	32	34	AR019430	1.21	0.049	43	1400	17600	100	2
AGSR0414	34	36	AR019431	1.54	0.058	38	1650	19900	100	2
AGSR0414	36	38	AR019432	1.71	0.071	39	2140	22100	100	bd
AGSR0414	38	40	AR019433	1.7	0.077	38	2430	21600	100	1
AGSR0414	40	42	AR019434	1.55	0.083	43	2390	21700	100	1
AGSR0414	42	44	AR019435	1.57	0.09	29	2280	17000	100	bd
AGSR0414	44	46	AR019436	1.31	0.072	26	1700	13900	bd	2
AGSR0414	46	48	AR019438	1.15	0.088	24	3950	11100	bd	2
AGSR0414	48	50	AR019439	0.697	0.066	16	4180	6300	bd	3
AGSR0414	50	52	AR019440	0.579	0.044	10	2710	4760	bd	3
AGSR0414	52	54	AR019441	0.513	0.036	11	2180	4070	bd	3
AGSR0414	54	56	AR019442	0.45	0.029	8	1680	3300	bd	5
AGSR0414	56	58	AR019443	0.358	0.021	5	1160	2630	bd	5
AGSR0414	58	60	AR019444	0.207	0.009	3	750	1730	bd	bd
AGSR0414	60	62	AR019445	0.229	0.011	3	1000	1850	bd	2
AGSR0414	62	64	AR019446	0.2	0.01	3	920	1610	bd	4
AGSR0414	64	66	AR019448	0.266	0.012	4	960	2890	bd	3
AGSR0414	66	68	AR019449	0.227	0.009	3	910	2480	bd	1
AGSR0414	68	70	AR019450	0.276	0.014	5	940	3150	bd	2
AGSR0414	70	72	AR019451	0.246	0.01	3	770	2570	bd	3
AGSR0414	72	74	AR019452	0.186	0.007	3	630	2010	bd	3
AGSR0414	74	76	AR019453	0.197	0.009	3	900	2770	bd	bd
AGSR0414	76	78	AR019454	0.208	0.009	3	780	3360	bd	bd
AGSR0414	78	80	AR019455	0.216	0.009	4	700	3520	bd	2
AGSR0414	80	82	AR019456	0.248	0.012	5	830	3080	bd	2
AGSR0414	82	84	AR019458	0.231	0.011	4	780	2530	bd	2
AGSR0414	84	86	AR019459	0.206	0.009	4	710	3060	bd	1
AGSR0414	86	88	AR019460	0.226	0.011	4	770	2810	bd	1
AGSR0414	88	90	AR019461	0.251	0.013	5	870	3160	bd	2
AGSR0414	90	92	AR019462	0.229	0.011	5	870	2930	bd	1
AGSR0414	92	94	AR019463	0.275	0.018	7	1080	2550	bd	1
AGSR0414	94	96	AR019464	0.228	0.012	5	860	2760	bd	3
AGSR0414	96	98	AR019465	0.219	0.011	5	850	2860	bd	2
AGSR0414	98	100	AR019466	0.255	0.012	5	960	2310	bd	1
AGSR0414	100	102	AR019468	0.247	0.011	4	920	1790	bd	1
AGSR0414	102	104	AR019469	0.216	0.009	4	890	950	bd	1
AGSR0414	104	106	AR019470	0.249	0.011	5	960	1080	bd	5
AGSR0414	106	108	AR019471	0.254	0.011	4	900	1080	bd	6
AGSR0414	108	110	AR019472	0.257	0.011	4	920	1070	bd	4
AGSR0414	110	112	AR019473	0.254	0.011	4	920	1130	bd	2
AGSR0414	112	114	AR019474	0.257	0.01	4	900	1030	bd	2
AGSR0414	114	116	AR019475	0.263	0.009	4	760	1050	bd	3
AGSR0414	116	118	AR019476	0.262	0.01	5	920	1040	bd	1
AGSR0414	118	120	AR019478	0.229	0.009	4	730	895	bd	8
AGSR0414	120	122	AR019479	0.212	0.008	4	790	905	bd	5
AGSR0414	122	124	AR019480	0.207	0.008	4	850	955	bd	1
AGSR0414	124	126	AR019481	0.247	0.01	5	940	1090	bd	1
AGSR0414	126	128	AR019482	0.268	0.01	5	1130	1180	bd	bd
AGSR0414	128	130	AR019483	0.73	0.018	9	2280	2300	bd	3
AGSR0414	130	132	AR019484	1.02	0.017	9	1110	3300	bd	6
AGSR0414	132	134	AR019485	0.804	0.015	7	760	3080	bd	2
AGSR0414	134	136	AR019486	0.267	0.011	5	900	1640	bd	1
AGSR0414	136	138	AR019488	0.242	0.01	5	860	1910	bd	bd
AGSR0414	138	140	AR019489	0.268	0.011	5	870	2080	bd	1
AGSR0414	140	142	AR019490	0.212	0.008	5	840	3610	bd	6
AGSR0414	142	144	AR019491	0.263	0.012	6	940	4740	bd	13
AGSR0414	144	146	AR019492	0.273	0.012	5	1010	5580	bd	2

Hole	From (m)	To (m)	Sample number	Ni (%)	Co (%)	Sc (g/t)	Mn (ppm)	Cr (ppm)	V (ppm)	Au (ppb)
AGSR0414	146	148	AR019493	0.263	0.015	6	1330	4690	bd	2
AGSR0414	148	150	AR019494	0.445	0.013	6	1220	5330	bd	bd
AGSR0414	150	152	AR019495	0.569	0.014	11	740	6720	bd	1
AGSR0414	152	154	AR019496	0.35	0.015	7	1270	6100	bd	bd
AGSR0414	154	156	AR019498	0.468	0.016	7	1000	6440	bd	bd
AGSR0414	156	158	AR019499	0.257	0.013	5	1030	4040	bd	1
AGSR0415	0	2	AR019504	0.026	0.004	21	390	480	100	16
AGSR0415	2	4	AR019505	0.258	0.008	15	520	3190	100	4
AGSR0415	4	6	AR019506	0.017	bd	23	140	1590	300	1
AGSR0415	6	8	AR019507	0.052	0.004	41	260	4110	400	3
AGSR0415	8	10	AR019508	0.054	0.005	30	240	2280	300	3
AGSR0415	10	12	AR019509	0.119	0.015	38	330	2560	300	4
AGSR0415	12	14	AR019510	0.108	0.012	32	190	2200	300	6
AGSR0415	14	16	AR019511	0.112	0.012	31	130	2330	300	51
AGSR0415	16	18	AR019512	0.112	0.01	30	120	1550	200	22
AGSR0415	18	20	AR019513	0.116	0.006	39	30	1880	200	5
AGSR0415	20	22	AR019515	0.133	0.015	34	270	2290	400	3
AGSR0415	22	24	AR019516	0.092	0.009	24	300	2120	300	1
AGSR0415	24	26	AR019517	0.149	0.011	20	710	3670	200	1
AGSR0415	26	28	AR019518	0.324	0.016	44	660	6010	200	5
AGSR0415	28	30	AR019519	0.643	0.014	75	630	8030	300	2
AGSR0415	30	32	AR019520	0.939	0.013	71	540	9380	300	3
AGSR0415	32	34	AR019521	0.922	0.013	66	570	10400	200	2
AGSR0415	34	36	AR019522	0.993	0.02	66	760	10500	200	3
AGSR0415	36	38	AR019523	0.951	0.038	54	1730	7330	100	1
AGSR0415	38	40	AR019525	1.05	0.041	47	1710	8650	100	bd
AGSR0415	40	42	AR019526	1.22	0.055	42	1820	11300	100	bd
AGSR0415	42	44	AR019527	1.12	0.066	36	1770	11700	100	bd
AGSR0415	44	46	AR019528	1.2	0.073	36	1710	10200	100	bd
AGSR0415	46	48	AR019529	1.36	0.168	34	14900	10100	100	bd
AGSR0415	48	50	AR019530	1.45	0.209	35	11700	14800	100	1
AGSR0415	50	52	AR019531	1.3	0.119	33	3510	17700	100	bd
AGSR0415	52	54	AR019532	1.35	0.121	34	4020	21200	100	bd
AGSR0415	54	56	AR019533	1.21	0.084	36	3040	28800	100	bd
AGSR0415	56	58	AR019535	1.24	0.061	35	2180	20900	100	1
AGSR0415	58	60	AR019536	1.11	0.048	27	1520	15000	100	1
AGSR0415	60	62	AR019537	1.16	0.041	21	1160	11500	100	6
AGSR0415	62	64	AR019538	1.04	0.033	16	940	8540	bd	28
AGSR0415	64	66	AR019539	0.903	0.025	12	580	6040	bd	44
AGSR0415	66	68	AR019540	0.791	0.027	12	850	4300	bd	11
AGSR0415	68	70	AR019541	0.651	0.035	8	2990	2400	bd	5
AGSR0415	70	72	AR019542	0.499	0.029	7	3410	1640	bd	3
AGSR0415	72	74	AR019543	0.555	0.028	6	2550	2380	bd	5
AGSR0415	74	76	AR019545	0.359	0.014	9	530	2360	bd	14
AGSR0415	76	78	AR019546	0.364	0.021	6	2860	1380	bd	9
AGSR0415	78	80	AR019547	0.44	0.027	5	3780	1470	bd	2
AGSR0416	0	2	AR019548	0.018	0.001	15	250	450	100	13
AGSR0416	2	4	AR019549	0.016	bd	19	140	1010	200	3
AGSR0416	4	6	AR019550	0.019	bd	23	120	1440	300	2
AGSR0416	6	8	AR019551	0.069	0.006	33	290	1780	200	3
AGSR0416	8	10	AR019552	0.111	0.015	41	360	2760	300	19
AGSR0416	10	12	AR019553	0.102	0.012	38	280	2080	200	9
AGSR0416	12	14	AR019555	0.102	0.014	28	490	1730	100	5
AGSR0416	14	16	AR019556	0.152	0.014	25	540	2200	300	5
AGSR0416	16	18	AR019557	0.137	0.011	23	160	2360	300	6
AGSR0416	18	20	AR019558	0.13	0.009	17	90	4160	600	4
AGSR0416	20	22	AR019559	0.133	0.009	29	80	2340	300	5
AGSR0416	22	24	AR019560	0.174	0.021	19	500	4510	300	2
AGSR0416	24	26	AR019561	0.279	0.014	44	290	10900	500	4
AGSR0416	26	28	AR019562	0.26	0.018	65	380	9980	200	7
AGSR0416	28	30	AR019563	0.309	0.022	62	470	10400	200	12
AGSR0416	30	32	AR019565	0.397	0.018	75	370	15700	200	5
AGSR0416	32	34	AR019566	0.511	0.045	77	600	13900	200	3
AGSR0416	34	36	AR019567	0.537	0.038	84	610	13900	200	4
AGSR0416	36	38	AR019568	0.666	0.027	102	550	17200	200	3
AGSR0416	38	40	AR019569	0.774	0.028	107	630	16500	200	3
AGSR0416	40	42	AR019570	0.869	0.027	109	650	18200	200	3
AGSR0416	42	44	AR019571	1.13	0.026	104	790	23900	200	2
AGSR0416	44	46	AR019572	0.879	0.021	88	850	20000	200	2
AGSR0416	46	48	AR019573	0.613	0.016	70	580	18200	200	2
AGSR0416	48	50	AR019575	0.359	0.01	52	430	12400	100	2
AGSR0416	50	52	AR019576	0.174	0.007	30	600	7340	100	5
AGSR0416	52	54	AR019577	0.163	0.01	17	510	7970	100	10
AGSR0416	54	56	AR019578	0.203	0.034	21	1550	10100	100	12
AGSR0416	56	58	AR019579	0.348	0.024	42	1100	12000	100	12
AGSR0416	58	60	AR019580	0.341	0.067	38	3570	11100	100	7
AGSR0416	60	62	AR019581	0.326	0.04	32	2310	11300	100	9
AGSR0416	62	64	AR019582	0.72	0.102	33	4860	17800	100	5
AGSR0416	64	66	AR019583	0.931	0.115	35	4990	20500	100	4
AGSR0416	66	68	AR019585	0.903	0.062	37	2580	24300	100	10
AGSR0416	68	70	AR019586	0.867	0.056	38	1880	26700	100	1050
AGSR0416	70	72	AR019587	0.992	0.053	36	1760	26200	100	886
AGSR0416	72	74	AR019588	0.751	0.046	28	1520	18200	100	269
AGSR0416	74	76	AR019589	0.792	0.054	33	1920	29300	100	64
AGSR0416	76	78	AR019590	0.842	0.059	34	2260	28500	100	43
AGSR0416	78	80	AR019591	0.81	0.066	33	2500	26400	100	59
AGSR0416	80	82	AR019592	0.867	0.068	38	2350	22300	100	50
AGSR0416	82	84	AR019593	0.841	0.089	37	4200	22300	100	56
AGSR0416	84	86	AR019595	0.886	0.089	29	5800	19000	100	85
AGSR0416	86	88	AR019596	0.85	0.083	36	2240	19700	100	95
AGSR0416	88	90	AR019597	1.06	0.105	33	1850	20200	100	80
AGSR0417	0	2	AR019598	0.063	0.006	18	310	1500	100	15
AGSR0417	2	4	AR019599	0.033	0.002	23	190	1190	100	6

Hole	From (m)	To (m)	Sample number	Ni (%)	Co (%)	Sc (g/t)	Mn (ppm)	Cr (ppm)	V (ppm)	Au (ppb)
AGSR0417	4	6	AR019600	0.029	0.001	24	140	1270	200	3
AGSR0417	6	8	AR019601	0.026	bd	26	110	1970	200	2
AGSR0417	8	10	AR019602	0.055	0.006	26	150	5450	300	2
AGSR0417	10	12	AR019603	0.075	0.013	19	230	12000	300	2
AGSR0417	12	14	AR019605	0.081	0.005	23	130	16200	400	2
AGSR0417	14	16	AR019606	0.074	0.002	20	150	20000	500	2
AGSR0417	16	18	AR019607	0.169	0.007	25	160	11100	200	3
AGSR0417	18	20	AR019608	0.34	0.011	47	190	10400	100	3
AGSR0417	20	22	AR019609	0.29	0.008	38	320	7570	100	4
AGSR0417	22	24	AR019610	0.507	0.008	43	440	11900	100	6
AGSR0417	24	26	AR019611	0.816	0.035	40	1320	11700	bd	4
AGSR0417	26	28	AR019612	1.06	0.049	43	1950	11000	100	4
AGSR0417	28	30	AR019613	1.04	0.044	44	1690	12000	100	5
AGSR0417	30	32	AR019615	0.932	0.041	36	1220	10900	100	4
AGSR0417	32	34	AR019616	0.8	0.037	33	980	13600	bd	9
AGSR0417	34	36	AR019617	0.744	0.043	29	1080	14300	bd	5
AGSR0417	36	38	AR019618	0.722	0.051	17	1030	9380	bd	5
AGSR0417	38	40	AR019619	0.935	0.051	16	1080	10500	bd	2
AGSR0417	40	42	AR019620	1.4	0.059	22	1340	15400	100	2
AGSR0417	42	44	AR019621	1.18	0.06	21	1170	11400	bd	2
AGSR0417	44	46	AR019622	0.896	0.047	21	1260	19100	bd	3
AGSR0417	46	48	AR019623	0.684	0.038	8	1730	6060	bd	3
AGSR0417	48	50	AR019625	0.478	0.02	5	1210	2700	bd	2
AGSR0417	50	52	AR019626	0.342	0.012	4	710	4010	bd	2
AGSR0417	52	54	AR019627	0.466	0.023	3	1260	3980	bd	11
AGSR0417	54	56	AR019628	0.304	0.018	4	1500	4340	bd	6
AGSR0417	56	58	AR019629	0.441	0.019	5	1090	10100	bd	10
AGSR0417	58	60	AR019630	0.513	0.016	7	760	11400	bd	20
AGSR0417	60	62	AR019631	0.767	0.024	20	870	18600	100	2
AGSR0417	62	64	AR019632	0.6	0.018	15	650	9570	bd	12
AGSR0417	64	66	AR019633	0.652	0.017	12	670	9220	bd	12
AGSR0417	66	68	AR019635	0.496	0.021	3	1870	4120	bd	10
AGSR0417	68	70	AR019636	0.445	0.019	3	1750	4500	bd	25
AGSR0418	0	2	AR019638	0.029	0.003	12	240	650	100	9
AGSR0418	2	4	AR019639	0.035	0.005	16	280	580	100	5
AGSR0418	4	6	AR019640	0.024	0.001	17	140	1180	100	2
AGSR0418	6	8	AR019641	0.029	0.001	18	70	3120	300	3
AGSR0418	8	10	AR019642	0.031	bd	16	60	2730	300	2
AGSR0418	10	12	AR019643	0.033	0.001	15	70	3540	300	3
AGSR0418	12	14	AR019645	0.069	0.011	30	430	9610	200	1
AGSR0418	14	16	AR019646	0.198	0.009	55	230	18300	100	1
AGSR0418	16	18	AR019647	0.203	0.014	71	220	18700	100	2
AGSR0418	18	20	AR019648	0.303	0.014	60	330	22100	100	2
AGSR0418	20	22	AR019649	0.3	0.019	39	550	22800	100	2
AGSR0418	22	24	AR019650	0.284	0.035	42	630	19200	100	2
AGSR0418	24	26	AR019651	0.324	0.031	42	350	10200	100	1
AGSR0418	26	28	AR019652	0.349	0.027	40	290	12100	100	3
AGSR0418	28	30	AR019653	0.482	0.027	39	350	12700	100	3
AGSR0418	30	32	AR019655	0.511	0.019	41	250	12200	100	4
AGSR0418	32	34	AR019656	0.824	0.038	28	580	20000	100	4
AGSR0418	34	36	AR019657	1.16	0.056	24	880	19400	100	5
AGSR0418	36	38	AR019658	0.689	0.036	21	620	13500	bd	5
AGSR0418	38	40	AR019659	0.673	0.037	20	600	13100	bd	6
AGSR0418	40	42	AR019660	0.646	0.046	19	1310	12300	bd	4
AGSR0418	42	44	AR019661	0.659	0.064	14	3310	9670	bd	3
AGSR0418	44	46	AR019662	0.639	0.064	16	2550	10900	bd	3
AGSR0418	46	48	AR019663	0.705	0.062	16	2230	11500	bd	3
AGSR0418	48	50	AR019665	1.12	0.088	13	3300	8650	bd	3
AGSR0418	50	52	AR019666	0.961	0.062	9	2790	4640	bd	4
AGSR0418	52	54	AR019667	0.867	0.053	8	2440	4000	bd	3
AGSR0418	54	56	AR019668	0.444	0.035	32	880	11800	100	3
AGSR0418	56	58	AR019669	0.661	0.038	8	1740	4470	bd	5
AGSR0418	58	60	AR019670	0.711	0.039	6	1870	4440	bd	12
AGSR0418	60	62	AR019671	0.445	0.024	4	1230	2480	bd	18
AGSR0418	62	64	AR019672	0.516	0.028	4	1310	3080	bd	27
AGSR0418	64	66	AR019673	0.391	0.019	3	1030	2410	bd	7
AGSR0418	66	68	AR019675	0.403	0.025	3	1440	2570	bd	8
AGSR0418	68	70	AR019676	0.513	0.035	4	1470	2780	bd	7
AGSR0418	70	72	AR019677	0.55	0.035	5	1560	2750	bd	34
AGSR0418	72	74	AR019678	0.337	0.02	4	1260	2130	bd	22
AGSR0418	74	76	AR019679	0.348	0.019	4	1380	2370	bd	34
AGSR0418	76	78	AR019680	0.236	0.01	3	930	1390	bd	7
AGSR0418	78	80	AR019681	0.238	0.008	3	700	1170	bd	bd
AGSR0418	80	82	AR019682	0.206	0.007	3	620	950	bd	1
AGSR0418	82	84	AR019683	0.215	0.007	3	710	1090	bd	1
AGSR0418	84	86	AR019685	0.23	0.009	4	770	1480	bd	bd
AGSR0418	86	88	AR019686	0.304	0.014	3	1290	855	bd	2
AGSR0418	88	90	AR019687	0.609	0.047	4	2970	2990	bd	105
AGSR0418	90	92	AR019688	0.463	0.026	5	1940	2840	bd	206
AGSR0418	92	94	AR019689	0.288	0.011	4	930	1340	bd	24
AGSR0418	94	96	AR019690	0.312	0.015	5	1030	1890	bd	24
AGSR0418	96	98	AR019691	0.283	0.012	4	930	1620	bd	15
AGSR0418	98	100	AR019692	0.235	0.009	3	800	1150	bd	6
AGSR0418	100	102	AR019693	0.243	0.009	3	820	1290	bd	2
AGSR0418	102	104	AR019695	0.32	0.013	4	1500	1550	bd	2
AGSR0418	104	106	AR019696	0.618	0.021	7	1430	3660	bd	43
AGSR0418	106	108	AR019697	1.43	0.033	16	2390	8500	bd	20
AGSR0418	108	110	AR019698	2.12	0.073	28	7010	14800	bd	5
AGSR0418	110	112	AR019699	2.12	0.106	29	7030	16300	bd	14
AGSR0418	112	114	AR019700	2.39	0.138	33	12200	17300	bd	4
AGSR0418	114	116	AR019701	1.95	0.089	29	6840	14800	bd	61
AGSR0418	116	118	AR019702	2.08	0.115	25	13700	12400	bd	48
AGSR0418	118	120	AR019703	1.88	0.294	19	37000	8460	bd	12

Hole	From (m)	To (m)	Sample number	Ni (%)	Co (%)	Sc (g/t)	Mn (ppm)	Cr (ppm)	V (ppm)	Au (ppb)
AGSR0418	120	122	AR019705	1.41	0.491	11	37100	4520	bd	7
AGSR0418	122	124	AR019706	0.998	0.298	11	14400	4470	bd	5
AGSR0418	124	126	AR019707	1.22	0.381	12	29700	4770	bd	4
AGSR0418	126	128	AR019708	1.29	0.349	15	29100	5920	bd	8
AGSR0418	128	130	AR019709	1.1	0.215	17	18800	7370	bd	14
AGSR0418	130	132	AR019710	0.965	0.13	14	10800	7390	bd	8
AGSR0418	132	134	AR019711	1.11	0.12	15	10400	8020	bd	15
AGSR0418	134	136	AR019712	1.5	0.112	18	9580	18100	bd	9
AGSR0418	136	138	AR019713	0.863	0.026	9	1350	11400	bd	16
AGSR0418	138	140	AR019715	1.45	0.249	22	6320	24000	100	5
AGSR0418	140	142	AR019716	0.443	0.061	6	2820	9010	bd	18
AGSR0418	142	144	AR019717	1.23	0.211	23	10400	26500	100	9
AGSR0418	144	146	AR019718	1.13	0.124	30	8020	30800	100	14
AGSR0418	146	148	AR019719	1.7	0.063	27	2880	32700	100	9
AGSR0418	148	150	AR019720	1.63	0.064	27	2030	29500	100	3
AGSR0418	150	152	AR019721	0.805	0.033	20	1250	20500	100	25
AGSR0418	152	154	AR019722	0.725	0.059	19	3610	13700	100	50
AGSR0418	154	156	AR019723	0.67	0.038	8	1960	9010	bd	9
AGSR0418	156	158	AR019725	0.618	0.026	6	1810	8290	bd	4
AGSR0418	158	160	AR019726	0.595	0.032	6	2240	8170	bd	5
AGSR0418	160	162	AR019727	0.445	0.02	6	1420	5660	bd	4
AGSR0418	162	164	AR019728	0.48	0.023	7	1890	6650	bd	5
AGSR0418	164	166	AR019729	0.314	0.021	5	2110	3330	bd	3
AGSR0418	166	168	AR019730	0.721	0.019	7	1550	4870	bd	2
AGSR0418	168	170	AR019731	0.875	0.02	7	1660	5100	bd	2
AGSR0418	170	172	AR019732	0.303	0.021	5	1990	2860	bd	2
AGSR0418	172	174	AR019733	0.29	0.019	5	1710	3150	bd	4
AGSR0418	174	176	AR019735	0.303	0.021	6	1580	3370	bd	5
AGSR0418	176	178	AR019736	0.317	0.029	5	2250	3130	bd	7
AGSR0418	178	180	AR019737	0.308	0.02	5	1550	2650	bd	3
AGSR0419	0	2	AR019738	0.021	0.002	12	290	435	100	7
AGSR0419	2	4	AR019739	0.032	0.004	14	270	525	100	10
AGSR0419	4	6	AR019740	0.025	0.001	14	180	695	100	3
AGSR0419	6	8	AR019741	0.026	0.001	19	110	1550	200	1
AGSR0419	8	10	AR019742	0.03	0.001	23	140	3020	300	1
AGSR0419	10	12	AR019743	0.056	0.003	35	160	4130	300	bd
AGSR0419	12	14	AR019745	0.08	0.005	36	280	3150	200	3
AGSR0419	14	16	AR019746	0.134	0.006	54	310	10500	200	bd
AGSR0419	16	18	AR019747	0.25	0.011	92	350	17300	100	bd
AGSR0419	18	20	AR019748	0.256	0.01	98	220	19000	100	1
AGSR0419	20	22	AR019749	0.332	0.008	87	160	20600	200	1
AGSR0419	22	24	AR019750	0.342	0.014	55	260	14200	200	1
AGSR0419	24	26	AR019751	0.373	0.019	53	160	12200	100	1
AGSR0419	26	28	AR019752	0.461	0.017	59	150	15700	300	1
AGSR0419	28	30	AR019753	0.429	0.017	47	190	12900	200	2
AGSR0419	30	32	AR019755	0.636	0.018	62	250	16300	100	2
AGSR0419	32	34	AR019756	0.557	0.016	57	220	15100	100	3
AGSR0419	34	36	AR019757	0.588	0.019	45	290	12400	100	2
AGSR0419	36	38	AR019758	0.749	0.022	51	330	15000	100	3
AGSR0419	38	40	AR019759	0.635	0.024	38	410	10000	100	2
AGSR0419	40	42	AR019760	0.799	0.047	26	1110	6890	bd	2
AGSR0419	42	44	AR019761	1.36	0.107	19	3220	4190	bd	2
AGSR0419	44	46	AR019762	0.893	0.063	18	2010	4590	bd	3
AGSR0419	46	48	AR019763	1.17	0.081	20	2870	4670	bd	3
AGSR0419	48	50	AR019765	1.08	0.068	18	2420	4140	bd	4
AGSR0419	50	52	AR019766	0.932	0.041	27	1400	7480	bd	4
AGSR0419	52	54	AR019767	0.98	0.034	14	1150	4980	bd	6
AGSR0419	54	56	AR019768	1.01	0.05	16	2240	5090	bd	4
AGSR0419	56	58	AR019769	0.802	0.127	11	13000	3780	bd	3
AGSR0419	58	60	AR019770	0.74	0.094	11	9300	3550	bd	3
AGSR0419	60	62	AR019771	0.711	0.072	8	5280	3370	bd	6
AGSR0419	62	64	AR019772	0.809	0.067	8	3360	3450	bd	9
AGSR0419	64	66	AR019773	0.749	0.039	9	2200	4120	bd	6
AGSR0419	66	68	AR019775	0.719	0.03	11	1630	4370	bd	3
AGSR0419	68	70	AR019776	1.23	0.047	32	1710	11700	100	1
AGSR0419	70	72	AR019777	1.55	0.052	32	1990	16000	100	1
AGSR0419	72	74	AR019778	2.02	0.086	31	3320	30000	100	1
AGSR0419	74	76	AR019779	1.61	0.112	35	4670	24300	100	1
AGSR0419	76	78	AR019780	1.53	0.126	34	5880	24600	100	1
AGSR0419	78	80	AR019781	1.72	0.189	34	7990	22800	100	bd
AGSR0419	80	82	AR019782	1.33	0.265	34	9670	22800	100	1
AGSR0419	82	84	AR019783	1.18	0.127	38	5290	22300	200	1
AGSR0419	84	86	AR019785	0.981	0.136	36	7000	21500	200	bd
AGSR0419	86	88	AR019786	1.56	0.772	33	46500	22200	200	2
AGSR0419	88	90	AR019787	1.86	1.08	38	74000	20100	200	2
AGSR0419	90	92	AR019788	1.64	0.655	44	58700	17900	200	2
AGSR0419	92	94	AR019789	1.58	0.59	44	43900	18700	200	2
AGSR0419	94	96	AR019790	1.4	0.431	43	26700	14000	200	2
AGSR0419	96	98	AR019791	1.91	0.475	39	26200	16200	200	2
AGSR0419	98	100	AR019792	2	0.53	35	29300	17900	100	3
AGSR0419	100	102	AR019793	2	0.461	34	24100	19100	100	1
AGSR0419	102	104	AR019795	1.4	0.305	37	15900	14600	200	2
AGSR0419	104	106	AR019796	1.38	0.275	37	15200	16600	200	bd
AGSR0419	106	108	AR019797	1.46	0.266	33	15800	21900	100	2
AGSR0419	108	110	AR019798	1.41	0.227	34	12200	19600	100	23
AGSR0419	110	112	AR019799	1.42	0.283	35	15500	18000	200	33
AGSR0419	112	114	AR019800	1.71	0.43	36	21700	16000	200	43
AGSR0419	114	116	AR019801	1.84	0.584	34	28800	12700	100	32
AGSR0419	116	118	AR019802	1.65	0.552	33	27800	12800	100	22
AGSR0419	118	120	AR019803	1.99	0.794	31	37200	10000	100	15
AGSR0419	120	122	AR019805	1.91	0.582	31	26200	11700	100	6
AGSR0419	122	124	AR019806	1.96	0.671	32	30500	12700	100	10
AGSR0419	124	126	AR019807	1.82	0.515	32	24100	14000	100	12

Hole	From (m)	To (m)	Sample number	Ni (%)	Co (%)	Sc (g/t)	Mn (ppm)	Cr (ppm)	V (ppm)	Au (ppb)
AGSR0419	126	128	AR019808	1.7	0.308	33	14100	16200	100	74
AGSR0419	128	130	AR019809	1.57	0.306	32	15100	17600	100	176
AGSR0419	130	132	AR019810	1.4	0.251	33	12500	18700	100	170
AGSR0419	132	134	AR019811	1.29	0.197	37	9410	20400	200	136
AGSR0419	134	136	AR019812	1.26	0.23	34	13900	21300	200	140
AGSR0419	136	138	AR019813	1.15	0.186	32	12300	23800	100	497
AGSR0419	138	140	AR019815	1.1	0.147	30	9490	22800	100	770
AGSR0419	140	142	AR019816	0.577	0.041	12	2110	10800	bd	639
AGSR0419	142	144	AR019817	0.25	0.021	7	1550	5290	bd	161
AGSR0419	144	146	AR019818	0.284	0.031	6	3710	4470	bd	49
AGSR0419	146	148	AR019819	0.317	0.037	7	4100	3060	bd	117
AGSR0419	148	150	AR019820	0.301	0.035	6	3270	2990	bd	230
AGSR0419	150	152	AR019821	0.297	0.033	6	2920	2480	bd	49
AGSR0419	152	154	AR019822	0.262	0.015	5	1240	2390	bd	62
AGSR0419	154	156	AR019823	0.273	0.022	5	2140	2470	bd	51
AGSR0419	156	158	AR019825	0.308	0.026	6	2170	2350	bd	29
AGSR0419	158	160	AR019826	0.42	0.02	7	1770	6540	bd	29
AGSR0419	160	162	AR019827	0.298	0.023	7	2020	5010	bd	10
AGSR0419	162	164	AR019828	0.373	0.021	7	1780	4140	bd	15
AGSR0419	164	166	AR019829	0.369	0.049	9	3400	5300	bd	51
AGSR0419	166	168	AR019830	0.453	0.045	11	2820	7080	bd	36
AGSR0419	168	170	AR019831	0.407	0.037	10	2520	6360	bd	35
AGSR0420	0	2	AR019832	0.019	0.001	12	340	415	100	8
AGSR0420	2	4	AR019833	0.026	0.003	14	280	520	100	7
AGSR0420	4	6	AR019835	0.029	0.002	18	180	895	100	3
AGSR0420	6	8	AR019836	0.095	0.004	31	210	10100	300	1
AGSR0420	8	10	AR019837	0.247	0.012	36	330	12300	200	1
AGSR0420	10	12	AR019838	0.204	0.022	21	520	12000	200	bd
AGSR0420	12	14	AR019839	0.163	0.026	21	490	15100	200	1
AGSR0420	14	16	AR019840	0.199	0.02	25	330	19200	200	1
AGSR0420	16	18	AR019841	0.202	0.013	26	180	17900	300	2
AGSR0420	18	20	AR019842	0.543	0.028	46	460	30200	100	4
AGSR0420	20	22	AR019843	0.761	0.027	25	1240	22800	100	11
AGSR0420	22	24	AR019845	0.66	0.022	24	1360	17800	100	5
AGSR0420	24	26	AR019846	0.692	0.028	25	790	14500	bd	12
AGSR0420	26	28	AR019847	0.725	0.031	22	790	15800	bd	31
AGSR0420	28	30	AR019848	0.783	0.036	17	760	13400	bd	7
AGSR0420	30	32	AR019849	0.605	0.027	13	840	9650	bd	7
AGSR0420	32	34	AR019850	0.596	0.03	12	1570	9600	bd	4
AGSR0420	34	36	AR019851	0.496	0.03	13	2470	8080	bd	2
AGSR0420	36	38	AR019852	0.486	0.035	11	2800	7770	bd	3
AGSR0420	38	40	AR019853	0.49	0.039	9	2390	7630	bd	2
AGSR0420	40	42	AR019855	0.601	0.049	10	3150	7040	bd	2
AGSR0420	42	44	AR019856	0.43	0.027	6	2510	5720	bd	1
AGSR0420	44	46	AR019857	0.39	0.017	6	1550	4510	bd	3
AGSR0420	46	48	AR019858	0.326	0.013	4	1380	3010	bd	1
AGSR0420	48	50	AR019859	0.401	0.015	4	1500	3290	bd	1
AGSR0420	50	52	AR019860	0.397	0.015	3	1660	3060	bd	1
AGSR0420	52	54	AR019861	0.385	0.015	4	1640	3000	bd	3
AGSR0420	54	56	AR019862	0.359	0.013	3	1510	3310	bd	4
AGSR0420	56	58	AR019863	0.409	0.019	5	1450	4500	bd	2
AGSR0420	58	60	AR019865	0.351	0.016	6	620	2040	bd	1
AGSR0420	60	62	AR019866	0.429	0.019	8	1400	3140	bd	6
AGSR0420	62	64	AR019867	0.285	0.012	5	1050	2230	bd	27
AGSR0420	64	66	AR019868	0.349	0.016	4	1210	1910	bd	41
AGSR0420	66	68	AR019869	0.388	0.015	3	1270	3030	bd	56
AGSR0420	68	70	AR019870	0.292	0.012	3	1180	2020	bd	37
AGSR0420	70	72	AR019871	0.263	0.01	2	960	2100	bd	87
AGSR0420	72	74	AR019872	0.333	0.015	3	1270	2090	bd	65
AGSR0420	74	76	AR019873	0.305	0.014	2	1720	2440	bd	182
AGSR0420	76	78	AR019875	0.3	0.017	9	1480	2380	bd	30
AGSR0420	78	80	AR019876	0.262	0.01	5	950	1230	bd	32
AGSR0420	80	82	AR019877	0.158	0.005	3	590	730	bd	5
AGSR0420	82	84	AR019878	0.228	0.008	4	720	1050	bd	5
AGSR0420	84	86	AR019879	0.244	0.009	4	740	1180	bd	7
AGSR0420	86	88	AR019880	0.263	0.009	4	760	1250	bd	5
AGSR0420	88	90	AR019881	0.225	0.008	4	700	1060	bd	1
AGSR0420	90	92	AR019882	0.257	0.009	4	730	1320	bd	3
AGSR0420	92	94	AR019883	0.275	0.011	5	850	1480	bd	3
AGSR0420	94	96	AR019885	0.272	0.011	5	790	1560	bd	2
AGSR0420	96	98	AR019886	0.242	0.009	5	770	1430	bd	1
AGSR0420	98	100	AR019887	0.243	0.009	4	740	1400	bd	2
AGSR0420	100	102	AR019888	0.219	0.008	4	750	1260	bd	4
AGSR0420	102	104	AR019889	0.2	0.007	7	660	1280	bd	2
AGSR0420	104	106	AR019890	0.206	0.007	7	770	1340	bd	2
AGSR0420	106	108	AR019891	0.267	0.008	5	1080	1490	bd	2
AGSR0420	108	110	AR019892	0.321	0.011	4	1080	3850	bd	2
AGSR0420	110	112	AR019893	0.255	0.011	5	930	4290	bd	3
AGSR0420	112	114	AR019895	0.244	0.012	7	940	3760	bd	bd
AGSR0420	114	116	AR019896	0.226	0.012	6	1210	4870	bd	3
AGSR0420	116	118	AR019897	0.602	0.014	6	1840	6030	bd	3
AGSR0420	118	120	AR019898	0.695	0.019	7	1450	7900	bd	2
AGSR0420	120	122	AR019899	0.713	0.022	9	1560	7840	bd	2
AGSR0420	122	124	AR019900	0.376	0.01	5	1440	4220	bd	2
AGSR0420	124	126	AR019901	0.264	0.011	4	1140	3930	bd	1
AGSR0420	126	128	AR019902	0.261	0.012	4	1040	3810	bd	1
AGSR0420	128	130	AR019903	0.257	0.013	6	1070	5330	bd	2
AGSR0420	130	132	AR019905	0.236	0.012	4	1160	4300	bd	6
AGSR0420	132	134	AR019906	0.521	0.017	6	1520	6580	bd	15
AGSR0420	134	136	AR019907	0.405	0.021	4	3130	3140	bd	7
AGSR0420	136	138	AR019908	0.347	0.013	5	1260	4270	bd	11
AGSR0420	138	140	AR019909	0.254	0.012	5	1000	3640	bd	8
AGSR0420	140	142	AR019910	0.263	0.011	6	980	3740	bd	13

Hole	From (m)	To (m)	Sample number	Ni (%)	Co (%)	Sc (g/t)	Mn (ppm)	Cr (ppm)	V (ppm)	Au (ppb)
AGSR0420	142	144	AR019911	0.269	0.013	5	1050	4910	bd	4
AGSR0420	144	146	AR019912	0.28	0.012	5	950	3330	bd	4
AGSR0420	146	148	AR019913	0.278	0.013	5	1020	3290	bd	4
AGSR0420	148	150	AR019915	0.251	0.01	5	840	3750	bd	11
AGSR0420	150	152	AR019916	0.249	0.012	5	930	3910	bd	7
AGSR0420	152	154	AR019917	0.23	0.009	6	730	2720	bd	9
AGSR0420	154	156	AR019918	0.259	0.013	6	1010	5090	bd	4
AGSR0420	156	158	AR019919	0.251	0.012	6	880	2980	bd	2
AGSR0420	158	160	AR019920	0.266	0.012	5	900	3440	bd	2
AGSR0420	160	162	AR019921	0.255	0.012	6	940	2860	bd	1
AGSR0420	162	164	AR019922	0.269	0.012	6	850	3110	bd	bd
AGSR0420	164	166	AR019923	0.271	0.012	5	940	2990	bd	1
AGSR0420	166	168	AR019925	0.268	0.012	5	970	2680	bd	4
AGSR0420	168	170	AR019926	0.273	0.012	5	1010	2370	bd	2
AGSR0421	0	2	AR019927	0.023	0.002	12	400	425	bd	9
AGSR0421	2	4	AR019928	0.037	0.005	17	340	670	100	3
AGSR0421	4	6	AR019929	0.018	bd	20	140	1380	100	1
AGSR0421	6	8	AR019930	0.026	0.001	18	160	2510	300	1
AGSR0421	8	10	AR019931	0.028	0.002	22	170	3400	400	1
AGSR0421	10	12	AR019932	0.041	0.002	23	90	3120	200	3
AGSR0421	12	14	AR019933	0.146	0.015	24	470	10800	400	1
AGSR0421	14	16	AR019935	0.223	0.032	28	820	17800	300	1
AGSR0421	16	18	AR019936	0.335	0.041	70	960	13600	300	bd
AGSR0421	18	20	AR019937	0.258	0.025	51	460	14100	300	16
AGSR0421	20	22	AR019938	0.507	0.032	44	360	15800	300	2
AGSR0421	22	24	AR019939	0.548	0.022	103	310	25400	300	3
AGSR0421	24	26	AR019940	0.553	0.022	95	430	22700	200	8
AGSR0421	26	28	AR019941	0.816	0.044	46	680	9690	200	3
AGSR0421	28	30	AR019942	1.03	0.062	37	760	11100	100	3
AGSR0421	30	32	AR019943	1.06	0.055	40	760	13600	100	4
AGSR0421	32	34	AR019945	0.827	0.043	21	1020	6310	bd	3
AGSR0421	34	36	AR019946	0.558	0.032	13	1170	3690	bd	2
AGSR0421	36	38	AR019947	0.582	0.04	13	1300	3990	bd	2
AGSR0421	38	40	AR019948	0.547	0.043	12	1340	3970	bd	2
AGSR0421	40	42	AR019949	0.546	0.05	13	2280	4400	bd	2
AGSR0421	42	44	AR019950	0.46	0.039	11	3060	3330	bd	1
AGSR0421	44	46	AR019951	0.545	0.046	12	4550	3780	bd	1
AGSR0421	46	48	AR019952	0.416	0.031	10	3070	3290	bd	2
AGSR0421	48	50	AR019953	0.476	0.03	10	2680	3010	bd	2
AGSR0421	50	52	AR019955	0.443	0.019	6	2210	2600	bd	bd
AGSR0421	52	54	AR019956	0.404	0.026	6	2940	3360	bd	1
AGSR0421	54	56	AR019957	0.565	0.067	10	7110	7820	bd	bd
AGSR0421	56	58	AR019958	0.486	0.045	13	3180	9770	bd	2
AGSR0421	58	60	AR019959	0.547	0.037	16	1880	13300	bd	2
AGSR0421	60	62	AR019960	0.941	0.062	23	2540	21600	100	bd
AGSR0421	62	64	AR019961	1.02	0.048	21	2010	18700	100	bd
AGSR0421	64	66	AR019962	0.654	0.041	26	1230	12900	100	7
AGSR0421	66	68	AR019963	0.67	0.037	40	1220	15600	100	4
AGSR0421	68	70	AR019965	0.961	0.038	42	1660	15300	100	1
AGSR0421	70	72	AR019966	0.951	0.033	47	1530	17500	200	1
AGSR0421	72	74	AR019967	0.962	0.03	61	1260	28700	200	bd
AGSR0421	74	76	AR019968	0.896	0.03	56	1220	28700	200	2
AGSR0421	76	78	AR019969	0.876	0.03	66	1370	27400	200	4
AGSR0421	78	80	AR019970	1.01	0.033	64	2040	28100	200	10
AGSR0421	80	82	AR019971	0.992	0.036	47	1970	38100	100	2
AGSR0421	82	84	AR019972	1.04	0.028	50	1820	28500	100	2
AGSR0421	84	86	AR019973	0.448	0.104	28	8200	13200	100	4
AGSR0421	86	88	AR019975	0.544	0.069	20	2450	9210	bd	2
AGSR0421	88	90	AR019976	0.62	0.161	18	16900	6940	bd	2
AGSR0421	90	92	AR019977	0.606	0.168	18	17600	7140	bd	bd
AGSR0421	92	94	AR019978	1.17	0.348	23	41600	8920	100	bd
AGSR0421	94	96	AR019979	1.21	0.229	34	16200	16000	100	bd
AGSR0421	96	98	AR019980	1.48	0.119	30	5380	37100	100	242
AGSR0421	98	100	AR019981	0.779	0.123	37	8390	19600	100	54
AGSR0421	100	102	AR019982	1.06	0.111	35	5520	27600	100	148
AGSR0421	102	104	AR019983	0.96	0.101	28	5270	17100	100	113
AGSR0421	104	106	AR019985	0.961	0.096	28	4330	20100	100	80
AGSR0421	106	108	AR019986	0.967	0.093	30	3110	15700	100	64
AGSR0421	108	110	AR019987	0.957	0.091	26	2730	14600	100	69
AGSR0421	110	112	AR019988	1.02	0.085	27	2150	23100	100	36
AGSR0421	112	114	AR019989	1.04	0.072	21	1650	20600	100	29
AGSR0421	114	116	AR019990	0.807	0.056	16	1330	13500	100	33
AGSR0421	116	118	AR019991	0.775	0.046	15	990	13500	100	10
AGSR0421	118	120	AR019992	0.753	0.041	16	790	13000	bd	7
AGSR0421	120	122	AR019993	0.5	0.025	11	2010	8910	bd	10
AGSR0421	122	124	AR019995	0.461	0.023	11	1250	8210	bd	11
AGSR0421	124	126	AR019996	0.621	0.023	12	920	10200	bd	25
AGSR0421	126	128	AR019997	0.497	0.021	15	610	8600	bd	28
AGSR0421	128	130	AR019998	0.526	0.027	19	1270	8150	bd	5
AGSR0422	0	2	AR019999	0.031	0.003	12	530	585	100	11
AGSR0422	2	4	AR020000	0.032	0.005	14	270	575	100	10
AGSR0422	4	6	AR020001	0.03	0.002	22	150	1230	100	3
AGSR0422	6	8	AR020002	0.023	0.001	30	140	3260	500	2
AGSR0422	8	10	AR020003	0.029	0.002	18	80	4550	500	4
AGSR0422	10	12	AR020004	0.074	0.008	16	350	8110	200	2
AGSR0422	12	14	AR020005	0.136	0.016	21	390	10400	100	3
AGSR0422	14	16	AR020006	0.156	0.022	20	630	10300	100	bd
AGSR0422	16	18	AR020007	0.181	0.028	24	470	16700	200	bd
AGSR0422	18	20	AR020008	0.25	0.017	34	290	19100	300	2
AGSR0422	20	22	AR020010	0.348	0.019	73	370	28300	200	2
AGSR0422	22	24	AR020011	0.676	0.041	45	510	10200	bd	bd
AGSR0422	24	26	AR020012	1.04	0.052	24	880	13000	bd	4
AGSR0422	26	28	AR020013	0.864	0.082	21	1920	11600	bd	3

Hole	From (m)	To (m)	Sample number	Ni (%)	Co (%)	Sc (g/t)	Mn (ppm)	Cr (ppm)	V (ppm)	Au (ppb)
AGSR0422	28	30	AR020014	1.04	0.124	23	3210	14000	bd	2
AGSR0422	30	32	AR020015	0.537	0.056	14	1560	6900	bd	2
AGSR0422	32	34	AR020016	0.397	0.04	9	1410	4290	bd	7
AGSR0422	34	36	AR020017	0.439	0.043	10	1740	4770	bd	6
AGSR0422	36	38	AR020018	0.542	0.052	11	3220	4900	bd	11
AGSR0422	38	40	AR020020	0.745	0.055	10	3730	5030	bd	10
AGSR0422	40	42	AR020021	0.625	0.036	7	2400	3180	bd	3
AGSR0422	42	44	AR020022	0.484	0.024	5	1750	1830	bd	11
AGSR0422	44	46	AR020023	0.568	0.027	5	2030	2220	bd	2
AGSR0422	46	48	AR020024	0.403	0.018	5	1270	1910	bd	3
AGSR0422	48	50	AR020025	0.299	0.013	4	780	1900	bd	3
AGSR0422	50	52	AR020026	0.272	0.011	3	730	1770	bd	1
AGSR0422	52	54	AR020027	0.27	0.011	3	700	1660	bd	1
AGSR0422	54	56	AR020028	0.228	0.008	3	610	1470	bd	2
AGSR0422	56	58	AR020030	0.184	0.006	3	540	1130	bd	4
AGSR0422	58	60	AR020031	0.197	0.006	3	600	1240	bd	6
AGSR0422	60	62	AR020032	0.197	0.006	2	620	1260	bd	6
AGSR0422	62	64	AR020033	0.19	0.006	3	590	1500	bd	9
AGSR0422	64	66	AR020034	0.188	0.006	3	590	1540	bd	4
AGSR0422	66	68	AR020035	0.195	0.006	3	590	1540	bd	3
AGSR0422	68	70	AR020036	0.191	0.006	4	570	1360	bd	26
AGSR0422	70	72	AR020037	0.188	0.006	4	570	1290	bd	12
AGSR0422	72	74	AR020038	0.217	0.007	4	640	1000	bd	4
AGSR0422	74	76	AR020040	0.183	0.006	3	580	960	bd	4
AGSR0422	76	78	AR020041	0.148	0.004	3	500	760	bd	2
AGSR0422	78	80	AR020042	0.231	0.007	4	650	1210	bd	1
AGSR0422	80	82	AR020043	0.209	0.007	4	590	1140	bd	1
AGSR0422	82	84	AR020044	0.155	0.005	3	570	750	bd	1
AGSR0422	84	86	AR020045	0.132	0.003	3	470	640	bd	2
AGSR0422	86	88	AR020046	0.178	0.006	4	570	1140	bd	2
AGSR0422	88	90	AR020047	0.163	0.005	3	590	940	bd	2
AGSR0422	90	92	AR020048	0.196	0.006	4	750	915	bd	5
AGSR0422	92	94	AR020050	0.143	0.005	3	650	740	bd	2
AGSR0422	94	96	AR020051	0.2	0.009	4	1110	1060	bd	8
AGSR0422	96	98	AR020052	0.343	0.029	4	2550	2580	bd	697
AGSR0422	98	100	AR020053	0.465	0.047	4	3340	4600	bd	1100
AGSR0422	100	102	AR020054	0.377	0.037	5	2920	3900	bd	503
AGSR0422	102	104	AR020055	0.496	0.042	11	1530	10200	bd	126
AGSR0422	104	106	AR020056	0.504	0.036	12	940	11300	bd	130
AGSR0422	106	108	AR020057	0.508	0.054	18	870	17200	100	9
AGSR0422	108	110	AR020058	0.529	0.052	17	880	14200	100	8
AGSR0422	110	112	AR020060	1.01	0.079	20	1830	24600	100	8
AGSR0422	112	114	AR020061	0.647	0.051	18	1430	13200	bd	163
AGSR0422	114	116	AR020062	0.856	0.229	16	7580	12500	bd	142
AGSR0422	116	118	AR020063	0.828	0.196	16	5980	10300	bd	151
AGSR0422	118	120	AR020064	0.694	0.11	15	3300	7530	bd	78
AGSR0422	120	122	AR020065	1.16	0.084	26	2360	12600	100	52
AGSR0422	122	124	AR020066	0.319	0.034	10	1050	4110	bd	29
AGSR0422	124	126	AR020067	0.648	0.065	17	1890	8620	bd	232
AGSR0422	126	128	AR020068	0.955	0.062	31	1300	13000	100	287
AGSR0422	128	130	AR020070	1.24	0.064	29	1290	11200	100	214
AGSR0422	130	132	AR020071	1.41	0.069	30	1290	10600	100	155
AGSR0422	132	134	AR020072	1.28	0.077	31	1570	11700	100	234
AGSR0422	134	136	AR020073	1.5	0.082	36	1300	17100	100	184
AGSR0422	136	138	AR020074	1.45	0.1	34	1210	17400	100	208
AGSR0422	138	140	AR020075	1.02	0.063	14	560	4540	bd	77
AGSR0422	140	142	AR020076	0.959	0.05	15	710	6430	bd	113
AGSR0422	142	144	AR020077	0.911	0.042	13	710	6130	bd	117
AGSR0422	144	146	AR020078	1.19	0.03	12	480	7950	bd	38
AGSR0422	146	148	AR020080	1.01	0.033	11	3870	5740	bd	31
AGSR0422	148	150	AR020081	1.01	0.028	10	2670	6900	bd	17
AGSR0422	150	152	AR020082	0.813	0.032	9	2240	9990	bd	26
AGSR0422	152	154	AR020083	0.483	0.027	10	3320	4860	bd	10
AGSR0422	154	156	AR020084	0.333	0.017	9	1380	5210	bd	7
AGSR0422	156	158	AR020085	0.295	0.017	11	910	5120	bd	10
AGSR0422	158	160	AR020086	0.293	0.015	7	1280	4350	bd	23

Appendix 5 – Collated intercepts, Pamela Jean Deeps

Parameters used to define nickel, cobalt, scandium, and gold intercepts at Pamela Jean Deeps

Parameter	Nickel	Cobalt	Scandium	Gold
Minimum cut-off	0.50 % Ni	0.08 % Co	50 g/t Sc	0.5 g/t
Minimum intercept thickness	2 m	2 m	2 m	2 m
Maximum internal waste thickness	4 m	4 m	4 m	4 m

Nickel, cobalt, and scandium intercepts from new drilling at Goongarrie South

All newly defined cobalt intercepts at Goongarrie South (calculated both from new data and historic data) were calculated using the following parameters:

- Intercepts based on nickel distributions were first calculated using 0.50 % nickel minimum cut-off, 2 m minimum intercept, and 4 m internal waste. Such parameters define broad intercepts that may be cobalt bearing or cobalt poor. Intercepts are considered of interest where cobalt values exceed 0.08%.
- Intercepts based on cobalt distributions are then calculated using a 0.10 % cobalt minimum cut-off, 2 m minimum intercept, and 4 m internal waste. All significant cobalt intercepts are hosted within the broader nickel-based intercepts and tend to define higher-grade, shorter intercepts.
- Where core loss was an issue, and where the thickness of core loss was less than the internal waste thickness, grades in zones of core loss were taken as the weighted average of the intervals immediately above and below the core loss interval in question. This provides grade distributions downhole that are consistent with mineralized zones, where nickel and cobalt grades are observed to change gradually rather than randomly downhole. By defining zones of core loss as being of a value between the interval above and the interval below, a similarly smooth transition in grades downhole is achieved. This method of estimated grade in zones of core loss is therefore considered the most suitable means of defining grade in such zones at Goongarrie South.
- Where an interval of core loss, through calculation, marked the beginning or end of a mineralized interval, this core loss interval was not included in that mineralization interval.

Scandium intercepts were defined by using a 50g/t scandium minimum cut-off, a 2 m minimum intercept, and a 4 m internal waste. Scandium intercept distributions do not show a consistent relationship to nickel and cobalt mineralization and are usually in the shallow subsurface but are only likely to be recovered where nickel and/or cobalt are present. As such, scandium intercepts are only presented where nickel intercepts are defined.

Gold intercepts show no relationship to nickel, cobalt nor scandium mineralization. Their association appears to be ad hoc.

Drillhole	Interval	NIckel Intercepts		Cobalt intercepts	Scandium intercepts (within Ni-Co mineralized zones)	Gold intercepts
AGSD0001	34 - 134.8 m	100.8 m at 1.00 % Ni and 0.08 % Co from 34 m	*including*	2 m at 1.02 % Ni and 0.11 % Co from 87 m	24.4 m at 51 g/t Sc from 34 m	
			and	7.2 m at 1.30 % Ni and 0.45 % Co from 95.6 m	8 m at 48 g/t Sc from 69 m	
			and	6 m at 1.40 % Ni and 0.22 % Co from 118 m	15.8 m at 52 g/t Sc from 106.2 m	
	140-2 - 165 m	24.8 m at 1.10 % Ni and 0.08 % Co from 140.2 m	*including*	8 m at 1.40 % Ni and 0.11 % Co from 152 m		
AGSR0001	8.3 - 32.3 m	24 m at 0.62 % Ni and 0.07 % Co from 8.3 m	*including*	4 m at 0.85 % Ni and 0.21 % Co from 14.3 m		
AGSR0185	20 - 46 m	26 m at 0.80 % Ni and 0.05 % Co from 20 m	*including*	4 m at 1.09 % Ni and 0.14 % Co from 38 m	6 m at 50 g/t Sc from 20 m	
AGSR0186	22 - 84 m	62 m at 0.92 % Ni and 0.04 % Co from 22 m	*including*	2 m at 1.40 % Ni and 0.08 % Co from 66 m	28 m at 57 g/t Sc from 22 m	
			and		12 m at 45 g/t Sc from 58 m	2 m at 0.40 g/t Au from 58 m
AGSR0187	24 - 84 m	60 m at 1.14 % Ni and 0.08 % Co from 24 m	*including*		58 m at 63 g/t Sc from 24 m	

Drillhole	Interval	Nickel Intercepts		Cobalt intercepts	Scandium intercepts (within Ni-Co mineralized zones)	Gold intercepts
			and	24 m at 1.27 % Ni and 0.14 % Co from 60 m		4 m at 0.48 g/t Au from 76 m
AGSR0190	36 - 60 m	24 m at 0.86 % Ni and 0.02 % Co from 36 m	*including*		24 m at 102 g/t Sc from 36 m	
	70 - 127 m	57 m at 1.04 % Ni and 0.10 % Co from 70 m	*including*	14 m at 0.82 % Ni and 0.2 % Co from 70 m	4 m at 50 g/t Sc from 78 m	
			and	16 m at 1.28 % Ni and 0.10 % Co from 90 m	2 m at 50 g/t Sc from 96 m	
AGSR0193	22 - 24 m	2 m at 0.53 % Ni and 0.03 % Co from 22 m				
	32 - 38 m	6 m at 0.55 % Ni and 0.06 % Co from 32 m				
AGSR0194	22 - 32 m	10 m at 0.61 % Ni and 0.02 % Co from 22 m				
AGSR0294	18 - 36 m	18 m at 0.98 % Ni and 0.08 % Co from 18 m	*including*	8 m at 0.98 % Ni and 0.12 % Co from 18 m	6 m at 50 g/t Sc from 20 m	
	46 - 48 m	2 m at 0.50 % Ni and 0.03 % Co from 46 m				
AGSR0295	20 - 30 m	10 m at 0.50 % Ni and 0.05 % Co from 20 m	*including*	2 m at 0.82 % Ni and 0.11 % Co from 20 m	2 m at 50 g/t Sc from 22 m	
	50 - 53 m	3 m at 0.66 % Ni and 0.02 % Co from 50 m				
AGSR0373	26 - 30 m	4 m at 0.71 % Ni and 0.08 % Co from 26 m	*including*	2 m at 0.78 % Ni and 0.12 % Co from 28 m		
AGSR0374	18 - 24 m	6 m at 0.50 % Ni and 0.02 % Co from 18 m				
AGSR0375	20 - 28 m	8 m at 0.68 % Ni and 0.04 % Co from 20 m	*including*		2 m at 60 g/t Sc from 20 m	
AGSR0377	22 - 31 m	9 m at 0.58 % Ni and 0.03 % Co from 22 m				
AGSR0380	18 - 25 m	7 m at 0.92 % Ni and 0.05 % Co from 18 m				
AGSR0411	22 - 54 m	32 m at 0.85 % Ni and 0.05 % Co from 22 m	*including*	2 m at 1.28 % Ni and 0.09 % Co from 38 m		
	76 - 96 m	20 m at 0.71 % Ni and 0.03 % Co from 76 m				
AGSR0412	22 - 60 m	38 m at 0.89 % Ni and 0.06 % Co from 22 m	*including*		8 m at 85 g/t Sc from 22 m	
			and	8 m at 1.17 % Ni and 0.13 % Co from 30 m	2 m at 50 g/t Sc from 36 m	
	68 - 72 m	4 m at 0.81 % Ni and 0.05 % Co from 68 m				
	76 - 78 m					2 m at 0.31 g/t Au from 76 m
	136 - 150 m	14 m at 0.78 % Ni and 0.04 % Co from 136 m	*including*	2 m at 1.13 % Ni and 0.11 % Co from 140 m		
AGSR0413	24 - 100 m	76 m at 1.11 % Ni and 0.09 % Co from 24 m	*including*		26 m at 58 g/t Sc from 24 m	
			and	12 m at 1.11 % Ni and 0.12 % Co from 44 m		
			and		30 m at 47 g/t Sc from 62 m	
			and	16 m at 1.37 % Ni and 0.22 % Co from 66 m		
			and	4 m at 1.37 % Ni and 0.13 % Co from 88 m		
	106 - 108 m	2 m at 0.52 % Ni and 0.01 % Co from 106 m				
	114 - 120 m	6 m at 0.66 % Ni and 0.01 % Co from 114 m				
AGSR0414	16 - 54 m	38 m at 1.01 % Ni and 0.10 % Co from 16 m	*including*		26 m at 60 g/t Sc from 16 m	
			and	8 m at 1.40 % Ni and 0.08 % Co from 40 m		
	128 - 134 m	6 m at 0.85 % Ni and 0.02 % Co from 128 m				
	150 - 152 m	2 m at 0.57 % Ni and 0.01 % Co from 150 m				
AGSR0415	28 - 74 m	46 m at 1.03 % Ni and 0.06 % Co from 28 m	*including*	10 m at 1.33 % Ni and 0.14 % Co from 46 m	30 m at 55 g/t Sc from 28 m	
AGSR0416	32 - 48 m	16 m at 0.75 % Ni and 0.03 % Co from 32 m	*including*		16 m at 94 g/t Sc from 32 m	
	62 - 90 m	28 m at 0.87 % Ni and 0.08 % Co from 62 m	*including*	4 m at 0.83 % Ni and 0.11 % Co from 62 m	26 m at 51 g/t Sc from 64 m	6 m at 0.74 g/t Au from 68 m
			and	8 m at 0.91 % Ni and 0.09 % Co from 82 m		
AGSR0417	22 - 48 m	26 m at 0.90 % Ni and 0.04 % Co from 22 m	*including*		2 m at 50 g/t Sc from 30 m	
	58 - 66 m	8 m at 0.63 % Ni and 0.02 % Co from 58 m				
AGSR0418	30 - 72 m	42 m at 0.67 % Ni and 0.04 % Co from 30 m	*including*	2 m at 1.12 % Ni and 0.09 % Co from 48 m		
	88 - 90 m	2 m at 0.61 % Ni and 0.05 % Co from 88 m				
	104 - 160 m	56 m at 1.29 % Ni and 0.14 % Co from 104 m	*including*	36 m at 1.40 % Ni and 0.2 % Co from 110 m		
	166 - 170 m	4 m at 0.80 % Ni and 0.02 % Co from 166 m				
AGSR0419	30 - 142 m	112 m at 1.30 % Ni and 0.26 % Co from 30 m	*including*	6 m at 1.14 % Ni and 0.08 % Co from 42 m	8 m at 53 g/t Sc from 30 m	
			and	4 m at 0.77 % Ni and 0.11 % Co from 56 m		

Drillhole	Interval	Nickel Intercepts		Cobalt intercepts	Scandium intercepts (within Ni-Co mineralized zones)	Gold intercepts
			and	68 m at 1.58 % Ni and 0.39 % Co from 72 m	32 m at 48 g/t Sc from 70 m	
			and		10 m at 48 g/t Sc from 108 m	
			and		14 m at 53 g/t Sc from 124 m	
						6 m at 0.64 g/t Au from 136 m
AGSR0420	18 - 34 m	16 m at 0.67 % Ni and 0.03 % Co from 18 m	*including*		2 m at 60 g/t Sc from 18 m	
	40 - 42 m	2 m at 0.60 % Ni and 0.05 % Co from 40 m				
	116 - 122 m	6 m at 0.67 % Ni and 0.02 % Co from 116 m				
	132 - 134 m	2 m at 0.52 % Ni and 0.02 % Co from 132 m				
AGSR0421	20 - 46 m	26 m at 0.66 % Ni and 0.04 % Co from 20 m	*including*		12 m at 70 g/t Sc from 20 m	
	54 - 130 m	76 m at 0.83 % Ni and 0.07 % Co from 54 m	*including*		18 m at 70 g/t Sc from 66 m	
			and	28 m at 0.91 % Ni and 0.14 % Co from 84 m	16 m at 54 g/t Sc from 96 m	
AGSR0422	22 - 46 m	24 m at 0.66 % Ni and 0.05 % Co from 22 m	*including*	4 m at 0.95 % Ni and 0.10 % Co from 26 m	2 m at 60 g/t Sc from 22 m	
	96 - 102 m					6 m at 0.77 g/t Au from 96 m
	104 - 152 m	48 m at 0.94 % Ni and 0.07 % Co from 104 m	*including*	8 m at 0.88 % Ni and 0.16 % Co from 114 m		
			and			2 m at 0.29 g/t Au from 126 m
			and	4 m at 1.48 % Ni and 0.09 % Co from 134 m		

Ardea Resources Limited

Appendix 6 – JORC Code, 2012 Edition, Table 1 report

Section 1 Sampling Techniques and Data

(Criteria in this section applies to all succeeding sections)

Criteria	JORC Code explanation	Commentary
Sampling techniques *Note: Due to the similarity of the deposit styles, procedures and estimations used this table represents the combined methods for all Ardea Resources (ARL) Nickel and cobalt Laterite Resources. Where data not collected by ARL has been used in the resource calculations, variances in techniques are noted.*	• *Nature and quality of sampling (e.g. cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc). These examples should not be taken as limiting the broad meaning of sampling.* • *Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used.* • *Aspects of the determination of mineralization that are Material to the Public Report.* • *In cases where 'industry standard' work has been done this would be relatively simple (e.g. 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases, more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralization types (e.g. submarine nodules) may warrant disclosure of detailed information.*	• All holes were sampled "in-principle" on a 2 metre down hole interval basis, with exceptions being made due to visual geological/mineralogical breaks, and end of hole final-lengths. All sampling lengths were recorded in ARL's standard core-sampling record spreadsheets. Sample condition, sample recovery and sample size were recorded for all drill-core samples collected by ARL. • The drill spacing was designed to augment historic drilling, bringing drill densities down from 80mE x 80mN to 40mE x 80mN. The drilling will also contribute to provide material for the purpose of metallurgical sampling and production of production of pilot marketing samples of cobalt sulphate and nickel sulphate. • Industry standard practice was used in the processing of samples for assay, with 2m intervals of RC chips collected in green plastic bags. As the drilling was within a 2012 JORC-compliant Indicated Ni-Co resource, prior knowledge of the resource peculiarities contributes and assists significantly to current interpretation of mineralization. • Assay of samples utilised standard laboratory techniques with standard ICP-AES undertaken on 50 gram samples for Au, Pt and Pd, and lithium borate fused-bead XRF analysis used for the remaining multi-element suite. Further details of lab processing techniques are found in Quality of assay data and laboratory tests below.
Drilling techniques	• *Drill type (e.g. core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc) and details (e.g. core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc).*	• In this most recent program, Ardea drilled the Goongarrie South deposit with 43 diamond drill holes on a varying MGA94 z51 northing grid-spacing of 80m at several localities (see Figure 2). Holes were vertical (-90 degree dip), designed to optimally intersect the sub-horizontal mineralization. RC drilling was performed with a face sampling hammer (bit diameter between 4½ and 5 ¼ inches) and samples were collected by either a cone (majority) or riffle splitter using 2 metre composites. Sample condition, sample recovery and sample size were recorded for all drill samples collected by ARL.
Drill sample recovery	• *Method of recording and assessing core and chip sample recoveries and results assessed.* • *Measures taken to maximise sample recovery and ensure representative nature of the samples.* • *Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.*	• RC chip sample recovery was recorded by visual estimation of the reject sample, expressed as a percentage recovery. Overall estimated recovery was approximately 80%, which is considered to be acceptable for nickel-cobalt laterite deposits. RC Chip sample condition recorded using a three code system, D=Dry, M=Moist, W=Wet. A small proportion of samples were moist or wet (11.5%), with the majority of these being associated with soft goethite clays, where water injection has been used to improve drill recovery. • Measures taken to ensure maximum RC sample recoveries included maintaining a clean cyclone and drilling equipment, using water injection at times of reduced air circulation, as well as regular communication with the drillers and slowing drill advance rates when variable to poor ground conditions are encountered.
Logging	• *Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.* • *Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc) photography.* • *The total length and percentage of the relevant intersections logged.*	• Drilling was undertaken for metallurgical purposes, and twinning comparison with previous historic RC holes. The level of logging detail utilised supports this type of review and was as follows: Visual geological logging was completed for all drilling both at the time of drilling (using standard Ardea laterite logging codes), and later over relevant met-sample intervals with a metallurgical-logging perspective. Geochemistry from historic data was used together with logging data to validate logged geological horizons. Nickel laterite profiles contain geochemically very distinct horizons and represent a sound validation tool against visual logging. The major part of the logging system was developed by Heron Resources Limited specifically for the KNP and was designed to facilitate future geo-metallurgical studies. It has been customised by Ardea Resources Limited as considered appropriate for recent developments. Planned drill hole target lengths were adjusted by the geologist during drilling. The geologist also oversaw all sampling and drilling practices. A mixture of ARL employees and contract geologists supervised all drilling. Quarter core of all drilling has been retained for reference. • Visual geological logging was completed for all RC drilling on 1 metre intervals. The logging system was developed by Heron Resources Limited specifically for the KNP and was designed to facilitate future geo-metallurgical studies. Logging was performed at the time of drilling, and planned drill hole target lengths adjusted by the geologist during drilling. The geologist also oversaw all sampling and drilling practices. A mixture of ARL employees and contract geologists supervised all drilling. A small selection of representative chips were also collected for every 1 metre interval

Criteria	JORC Code explanation	Commentary
		and stored in chip-trays for future reference. Only drilling contractors with previous nickel laterite experience and suitable rigs were used. • The geological legend used by ARL is a qualitative legend designed to capture the key physical and metallurgical features of the nickel-cobalt laterite mineralization. Logging captured the colour, regolith unit and mineralization style, often accompanied by the logging of protolith, estimated percentage of free silica, texture, grain size and alteration. Logging correlated well with the geochemical algorithm developed by Heron Resources Limited for the Yerilla Nickel Project for material type prediction from multi-element assay data.
Sub-sampling techniques and sample preparation	• *If core, whether cut or sawn and whether quarter, half or all core taken.* • *If non-core, whether riffled, tube sampled, rotary split, etc and whether sampled wet or dry.* • *For all sample types, the nature, quality and appropriateness of the sample preparation technique.* • *Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.* • *Measures taken to ensure that the sampling is representative of the in situ material collected, including for instance results for field duplicate/second-half sampling.* • *Whether sample sizes are appropriate to the grain size of the material being sampled.*	• 2 metre (and rarely 1 metre) composite samples were recovered using a 15:1 rig mounted cone splitter or trailer mounted riffle splitter during drilling into a calico sample bag. Sample target weight was between 2 and 3kg. In the case of wet clay samples, grab samples taken from sample return pile, initially into a calico sample bag. Wet samples stored separately from other samples in plastic bags and riffle split once dry. • QAQC was employed. A standard, blank or duplicate sample was inserted into the sample stream 10 metres on a rotating basis. Standards were either quantified industry standards, or standards made from homogenised bulk samples of the mineralization being drilled (in the case of the Yerilla project). Every 30th sample a duplicate sample was taken using the same sample sub sample technique as the original sub sample. Sample sizes are appropriate for the nature of mineralization.
Quality of assay data and laboratory tests	• *The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.* • *For geophysical tools, spectrometers, handheld XRF instruments, etc, the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.* • *Nature of quality control procedures adopted (e.g. standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (i.e. lack of bias) and precision have been established.*	• All Ardea samples were submitted to Kalgoorlie ALS laboratories and transported to ALS Perth, where they were pulverised. Analysis at ALS Perth was by ICP utilising a 50g charge (lab method PGM-ICP24) for PGM suite elements (Au, Pt, Pd). Additional analysis was undertaken by sending subsamples to ALS Brisbane where analysis by silicate fusion / XRF analysis (lab method ME-XRF12n) for multiple grade attributes for laterite ores (Al2O3, As, BaO, CaO, Cl, Co, Cr2O3, Cu, Fe2O3, Ga, K2O, MgO, MnO, Na2O, Ni, P2O5, Pb, Sc, SiO2, SO3, SrO, TiO2, V2O5, Zn, ZrO2). Fusion / XRF analysis is an industry standard method used to analyse nickel laterite ores and ALS is a reputable commercial laboratory with extensive experience in assaying nickel laterite samples from numerous Western Australian nickel laterite deposits. • ALS routinely inserts analytical blanks, standards and duplicates into the client sample batches for laboratory QAQC performance monitoring. • Ardea also inserted QAQC samples into the sample stream at a 1 in 10 frequency, alternating between blanks (industrial sands) and standard reference materials. Additionally, a review was conducted for geochemical consistency between historically expected data, recent data, and geochemical values that would be expected in a nickel laterite profile. • All of the QAQC data has been statistically assessed. There were rare but explainable inconsistencies in the returning results from standards submitted, and it has been determined that levels of accuracy and precision relating to the samples are acceptable.
Verification of sampling and assaying	• *The verification of significant intersections by either independent or alternative company personnel.* • *The use of twinned holes.* • *Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.* • *Discuss any adjustment to assay data.*	• All Ardea samples were submitted to Kalgoorlie ALS laboratories and transported to ALS Perth, where they were pulverised. Analysis at ALS Perth was by ICP utilising a 50g charge (lab method PGM-ICP24) for PGM suite elements (Au, Pt, Pd). Additional analysis was undertaken by sending subsamples to ALS Brisbane where analysis by silicate fusion / XRF analysis (lab method ME-XRF12n) for multiple grade attributes for laterite ores (Al2O3, As, BaO, CaO, Cl, Co, Cr2O3, Cu, Fe2O3, Ga, K2O, MgO, MnO, Na2O, Ni, P2O5, Pb, Sc, SiO2, SO3, SrO, TiO2, V2O5, Zn, ZrO2). Fusion / XRF analysis is an industry standard method used to analyse nickel laterite ores and ALS is a reputable commercial laboratory with extensive experience in assaying nickel laterite samples from numerous Western Australian nickel laterite deposits. • ALS routinely inserts analytical blanks, standards and duplicates into the client sample batches for laboratory QAQC performance monitoring. • Ardea also inserted QAQC samples into the sample stream at a 1 in 20 frequency, alternating between duplicates splits, blanks (industrial sands) and standard reference materials. • Additionally, a review was conducted for geochemical consistency between historically expected data, recent data, and geochemical values that would be expected in a nickel laterite profile. • All of the QAQC data has been statistically assessed. There were some inconsistencies in the returning results from standards submitted, relating to the XRF analysis suite. This has been thoroughly investigated with the conclusion that either some standards were not correctly identified and recorded on submission, or time/external influence has had an impact on some of the quality of the values standards, as figures reported for the relevant errant standards were significantly different to the normal recognisable standard values. Ardea has undertaken its own

Criteria	JORC Code explanation	Commentary
		further in-house review of QAQC results of the ALS routine standards, 100% of which returned within acceptable QAQC limits. This fact combined with the fact that the data is demonstrably consistent and repeated for expected Ni/Co values within the lateritic ore profiles of both reported areas and is also consistent with nearby abundant historic drilling data, has meant that the results are considered to be acceptable and suitable for reporting.
Location of data points	• *Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.* • *Specification of the grid system used.* • *Quality and adequacy of topographic control.*	• All drill holes are to be surveyed using an RTK DGPS system with either a 3 or 7 digit accuracy. The coordinates are stored in the exploration database referenced to the MGA Zone 51 Datum GDA94. • All holes drilled as part of the Goongarrie South program were vertical. No holes were down-hole surveyed except at EOH. The sub-horizontal orientation of the mineralization, combined with the soft nature of host material resulted in minimal deviation of vertical diamond drill holes. • The grid system for all models is GDA94. Where historic data or mine grid data has been used it has been transformed into GDA94 from its original source grid via the appropriate transformation. Both original and transformed data is stored in the digital database. • A DGPS pickup up of drill collar locations is considered sufficiently accurate for reporting of resources, but is not suitable for mine planning and reserves.
Data spacing and distribution	• *Data spacing for reporting of Exploration Results.* • *Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.* • *Whether sample compositing has been applied.*	• The drill spacing was designed to augment historic drilling, bringing drill densities down from 80mE x 80mN to 40mE x 80mN. The program to date is part of a broader program. All proposed drilling has been completed at Elsie South only. Drilling continues at all other deposits. • Given the homogeneity of this style of orebody, the spacing is, for bulk-scale metallurgical work and probable mining techniques, considered sufficient. • Sample compositing has not been applied to the newly collected data.
Orientation of data in relation to geological structure	• *Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.* • *If the relationship between the drilling orientation and the orientation of key mineralized structures is considered to have introduced a sampling bias, this should be assessed and reported if material.*	• All drill holes in this program which are vertical and give a true width of the regolith layers and mineralization within the modelled resource. The inclined holes are designed to test steep structures rather than regolith thickness and in all cases have sufficient adjoining vertical holes which quantify regolith true thickness • On a local scale, there is some geological variability in the northern most drill line (6669600mN) due to a probable shear structure. However, this local variability is not considered to be significant for the project overall, but will have local effects on mining and scheduling later in the project life. As the detailed shape of the orebody has already been well defined by an abundance of nearby resource drill holes (including the northern section) it is no bias is expected to be introduced from data pertaining to these drill holes with reference to mineralized structures.
Sample security	• *The measures taken to ensure sample security.*	• All samples were collected and accounted for by ARL employees/consultants during drilling. All samples were bagged into calico plastic bags and closed with cable ties. Samples were transported to Kalgoorlie from logging site by ARL employees/ consultants and submitted directly to ALS Kalgoorlie. • The appropriate manifest of sample numbers and a sample submission form containing laboratory instructions were submitted to the laboratory. Any discrepancies between sample submissions and samples received were routinely followed up and accounted for.

Audits or reviews	• *The results of any audits or reviews of sampling techniques and data.*	• ARL has periodically conducted internal reviews of sampling techniques relating to resultant exploration datasets, and larger scale reviews capturing the data from multiple drilling programmes within the KNP.
		• Internal reviews of the exploration data included the following:
		  • Unsurveyed drill hole collars (less than 1% of collars).
		  • Drill Holes with overlapping intervals (0%).
		  • Drill Holes with no logging data (less than 2% of holes).
		  • Sample logging intervals beyond end of hole depths (0%).
		  • Samples with no assay data (from 0 to <5% for any given project, usually
		• related to issues with sample recovery from difficult ground conditions,
		• mechanical issues with drill rig, damage to sample in transport or sample preparation).
		  • Assay grade ranges.
		  • Collar coordinate ranges
		  • Valid hole orientation data.
		• The ALS Laboratory was visited by ARL staff in 2016, and the laboratory processes and procedures were reviewed at this time and determined to be robust.

Section 2 - Reporting of Exploration Results

(Criteria listed in the preceding section also apply to this section.)

Criteria	JORC Code explanation	Commentary
Mineral tenement and land tenure status	• *Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.* • *The security of the tenure held at the time of reporting along with any known impediments*	• The tenement on which the Goongarrie South drilling was undertaken is M29/272. • The tenement and land tenure status for the KNP prospect areas containing continuous cobalt rich laterite mineralization is summarised in Table 3 following and in the Ardea Prospectus, section 9 "Solicitor's Report on Tenements".
Exploration done by other parties	• *Acknowledgment and appraisal of exploration by other parties.*	• The Goongarrie South deposit was initially discovered by Heron Resources Ltd and subsequently drilled by Vale Inco Limited in a Joint Venture. Much historic assessment of the Black Range Project was undertaken by Heron Resources Limited.
Geology	• *Deposit type, geological setting and style of mineralization.*	• The KNP nickel-cobalt laterite mineralization developed during the weathering and near surface enrichment of Archaean-aged olivine-cumulate ultramafic units. The mineralization is usually within 60 metres of surface and can be further subdivided on mineralogical and metallurgical characteristics into upper iron-rich material and lower magnesium-rich material based on the ratios of iron to magnesium. The deposits are analogous to many weathered ultramafic-hosted nickel-cobalt deposits both within Australia and world-wide. • Cobalt-rich mineralization is typically best developed in iron-rich material in regions of deep weathering in close proximity to major shear zones or transfer shear structures and to a lesser extent as thin zones along the interface of ferruginous and saprolite boundaries at shallower depths proximal to shear structures. • The Cobalt Zone is associated with a distinctive geo-metallurgical type defined as "Clay Upper Pyrolusitic". Mineralogy is goethite, gibbsite and pyrolusite (strictly "asbolite" or "cobaltian wad"). The Cobalt Zones typically occur as sub-horizontal bodies at a palaeo-water table within the KNP (late stage supergene enrichment). This material is particularly well developed at Goongarrie South.
Drill hole Information	• *A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes:* • *easting and northing of the drill hole collar* • *elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar* • *dip and azimuth of the hole* • *down hole length and interception depth* • *hole length.*	• All holes drilled in this most recent program are listed in "Appendix 1 – Collar location data".
Drill hole Information	• *If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.*	• All assay data relating to the metals of interest at Goongarrie South, namely cobalt, nickel, Sc, and chromium, are listed in "Appendix 2 – Assay results". Other elements were assayed but have not been reported here. They are of use and of interest from a scientific and metallurgical perspective, but are not considered material and their exclusion does not detract from the understanding of this report.

Data aggregation methods	• *In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (e.g. cutting of high grades) and cut-off grades are usually Material and should be stated.*
	• *Where aggregate intercepts incorporate short lengths of high-grade results and longer lengths of low-grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.*
	• *The assumptions used for any reporting of metal equivalent values should be clearly stated.*
		• Most drill hole samples have been collected over 2m down hole intervals.
		• All newly defined nickel and cobalt intercepts at Goongarrie South were calculated using the following parameters:
		  • Intercepts based on nickel distributions were first calculated using 0.50 % nickel minimum cut-off, 2 m minimum intercept, and 4 m internal waste. Such parameters define broad intercepts that may be cobalt bearing or cobalt poor. Intercepts are considered of interest where cobalt values exceed 0.08%.
		  • Intercepts based on cobalt distributions are then calculated using a 0.10 % cobalt minimum cut-off, 2 m minimum intercept, and 4 m internal waste. All significant cobalt intercepts are hosted within the broader nickel-based intercepts and tend to define higher-grade, shorter intercepts.
		  • Where core loss was an issue, and where the thickness of core loss was less than the internal waste thickness, grades in zones of core loss were taken as the weighted average of the intervals immediately above and below the core loss interval in question. This provides grade distributions downhole that are consistent with mineralized zones, where nickel and cobalt grades are observed to change gradually rather than randomly downhole. By defining zones of core loss as being of a value between the interval above and the interval below, a similarly smooth transition in grades downhole is achieved. This method of estimated grade in zones of core loss is therefore considered the most suitable means of defining grade in such zones at Goongarrie South.
		  • Where an interval of core loss, through calculation, marked the beginning or end of

Criteria	JORC Code explanation	Commentary
		a mineralized interval, this core loss interval was not included in that mineralization interval. • Sc intercepts were defined by using a 50g/t Sc minimum cut-off, a 2 m minimum intercept, and a 4 m internal waste. Sc intercept distributions do not show a consistent relationship to nickel and cobalt mineralization and are usually in the shallow subsurface. • Assay compositing techniques were not used in this assessment. • No metal equivalent calculations have been used in this assessment.
Relationship between mineralization widths and intercept lengths	• *These relationships are particularly important in the reporting of Exploration Results.* • *If the geometry of the mineralization with respect to the drill hole angle is known, its nature should be reported.* • *If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (e.g. 'down hole length, true width not known').*	• The nickel-cobalt laterite mineralization at Goongarrie South has a strong global sub-horizontal orientation. • All drill holes are vertical. • All drill holes intersect the mineralization at approximately 90°to its orientation
Diagrams	• *Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.*	• Maps and sections of the nickel and cobalt mineralization are shown within the report. Every drill hole on every section drilled is shown.
Balanced reporting	• *Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.*	• Not applicable to this report. All results are report either in the text or in the associated appendices. Examples of high-grade mineralization are labelled as such.
Other substantive exploration data	• *Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.*	• No other data are, at this stage, known to be either beneficial or deleterious to recovery of the metals reported. Uncertainties surrounding the possibility of recovery of the metals of interest are noted prominently in the report.
Further work	• *The nature and scale of planned further work (e.g. tests for lateral extensions or depth extensions or large-scale step-out drilling).* • *Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.*	• Further drilling is likely to be undertaken at Goongarrie South but has not yet been defined. Further drilling could include infill drilling as well as extension of lines to the north and south as appropriate. • Metallurgical assessment of all metals of interest at Goongarrie South will be undertaken during the Pre-Feasibility Study (PFS) which has commenced on the KNP Cobalt Zone.